# **AIR QUALITY ASSESSMENT REPORT**

Ontario Northland Northlander Passenger Rail Timmins-Porcupine Station Transit and Rail Project Assessment Process

March 22, 2025

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# **TABLE OF CONTENTS**

1.0 l	ntroduction	1
1.1	O. Reg. 231/08: Transit and Rail Project Assessment Process (TRPAP)	1
1.2	Study Area	3
1	2.1 Timmins-Porcupine Station Site Description	4
1.3	Study Objectives	4
1.4	Applicable Legislation / Guidance Documents	4
1.5	Ontario Ambient Air Quality Criteria (AAQC) and Canadian Ambient Air Quality Standards (CAAQS)	5
1.6	General Assessment Methodology	7
2.0 B	ackground Conditions and Air Quality	8
2.1	Climate	8
2.2	Air Quality - Atmospheric Chemistry	10
2.3	Selection of Monitoring Stations	12
3.0 L	ocal Air Quality Assessment	14
3.1	Overview - Train Station Operations	14
3.2	Sensitive Receptors in the Study Area	16
3.3	Road Traffic Data	18
3.4	Motor Vehicle Emissions Rates	18
3.5	Air Dispersion Modelling Using AERMOD	18
4.0 0	ireenhouse Gas Emissions	21
5.0 N	Aodelling Results	22
5.1	Worst-Case Analysis	22
5	1.1 Methodology	22
5	1.2 Results	22
	5.1.2.1 Nitrogen Dioxide	22
	5.1.2.2 PM2.5	23
	5.1.2.3 Benzene	23
6.0 C	onclusions	26
7.0 S	ummary of Potential Effects, Mitigation and Monitoring	27
8.0 R	leferences	31





# FIGURES

Figure 1: Study Area	3
Figure 2: Timmins – Porcupine Station Site, Looking South	4
Figure 3: Historical Wind Data	8
Figure 4: Monitoring Station Locations for Background Concentrations	13
Figure 5: Sensitive Receptors	17

# TABLES

Table 1: Project Components	2
Table 2: Summary of Ambient Air Quality Criteria / Standards	6
Table 3: Locomotive Emission Standards	15
Table 4: Source Summary Table	20
Table 5: Summary of Modelling Results	25
Table 6. Summary of Air Quality Mitigation Measures, Monitoring & Commitments	28

# **APPENDICES**

# **Appendix A: AERMOD Appendix**

- A1 Spec Sheets
- **A2 Dispersion Modelling**
- **A3 Controlling Contaminants**
- A4 Emission Rate Sample Calculations
- A5 AERMOD Summary Report

**Appendix B: MOVES4 Emissions Rates** 

**Appendix C: Fugitive Dust Best Management Plan** 





#### EXECUTIVE SUMMARY

#### INTRODUCTION

The Ontario Northland Transportation Commission (Ontario Northland) is an agency of the Province of Ontario responsible for providing efficient, safe, and reliable transportation services in Northern Ontario. Current services include inter-community bus passenger and bus parcel delivery services, freight rail services that connect Northeastern Ontario to other markets across Canada and around the world, and passenger rail service on the Polar Bear Express. The Polar Bear Express provides rail service connecting Cochrane to Moosonee and the Communities of the James Bay Coast since 1932. Previously, Ontario Northland operated the Northlander passenger rail service between Toronto and Cochrane, however, this service was discontinued in 2012.

The Government of Ontario has issued direction to Ontario Northland to reinstate passenger rail service between Toronto (Union Station) and Northeastern Ontario via the Northlander Passenger Rail (NPR) (the Project).

#### O. REG. 231/08: TRANSIT AND RAIL PROJECT ASSESSMENT PROCESS (TRPAP)

The proposed Timmins-Porcupine Station is subject to an environmental assessment study under *Ontario Regulation 231/08: Transit and Rail Projects Assessment Process* (February 16, 2024). The scope of the TRPAP examines the potential environmental effects associated with the new Timmins-Porcupine Station. In addition, the environmental impact assessment studies also consider the area of land adjacent to the proposed station where a future bus maintenance and storage facility may be built. At the time of preparing this EPR, the decision to build the bus facility was not yet definitive, and therefore an engineering design was not completed. Should the bus facility go forward in the future, the environmental impact assessment studies undertaken as part of the TRPAP will need to be revisited and updated, as required. These updated/additional impact assessment studies will be carried out as part of completing an Environmental Project Report (EPR) Addendum process (as per O. Reg. 231/08), which would also entail Ontario Northland carrying out additional public, stakeholder, and Indigenous Communities consultation. It should be noted that this Air Quality Report will be updated and augmented to include a full air quality modelling assessment of the bus maintenance and storage facility as part of the EPR Addendum process, if this component of the project moves forward in the future.

#### STUDY AREA

The boundaries of the TRPAP study area are depicted in **Figure 1.** The proposed station site is located on the southeast side of Falcon Street, to the east of Gervais Street North, and to the north of King Street (TransCanada Highway 101). Highway 101 veers to the north while Falcon Street curves to the east, and as such, these roads intersect and bound the site farther to the northeast. Vehicular access is from Falcon Street.

#### SCOPE OF AIR QUALITY ASSESSMENT

An Air Quality Impact Assessment was completed to characterize existing conditions and determine the impact of the Project on air quality. The scope of this Air Quality Assessment Report includes the following:

- Potential operational air quality effects of the project;
- Potential construction phase air quality effects of the project.

#### **OVERVIEW OF BACKGROUND AIR QUALITY**

A review of ambient background air pollutant levels was conducted to determine existing air quality at the subject site. **Figure 3** provides the location of the nearest Monitoring Stations. The nearest stations that measure NO<sub>2</sub> and PM<sub>2.5</sub> are Sault Ste. Marie, Sudbury, and North Bay, with Sudbury as the closest, while the nearest station



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that measures Benzene is Newmarket. As such, data from Sudbury was used for NO<sub>2</sub> and PM<sub>2.5</sub> while data from Newmarket was used for Benzene. Note: both MECP and NAPS monitoring stations were considered.

Additionally, it is important to note that Timmins, Sudbury, and Newmarket have similar land uses, which further supports the applicability and representativeness of this data for the air quality study. All three locations have a variety of housing options, including single-family homes, townhouses, and apartments. Each city has commercial areas with retail stores, offices, and service businesses. Timmins and Sudbury have significant industrial activities, particularly in mining and manufacturing, while Newmarket has light industrial activities and business parks. All three locations prioritize recreational spaces, with parks, trails, and recreational facilities available for residents.

#### SENSITIVE RECEPTORS

Two sensitive receptors were located at Pete Landers Park, one in the baseball infield and one in the baseball outfield. Further, a sensitive receptor was located at the Frank P. Whitney Public School. Six sensitive receptors were selected as representative of the residences around the proposed location of the station, as depicted in **Figure 4.** The residential receptors were identified by locating residences that are within 500 m of the proposed station. Contaminant concentrations are similar when in the same vicinity. The nine receptors selected represent the most sensitive and closest locations, providing a conservative basis for the analysis. Receptors located farther from the station will experience a diminished impact from the "build" scenario.

#### POTENTIAL OPERATIONAL AIR QUALTY EFFECTS

#### Emissions from Roads

The roads within influence distance of the site, Falcon Street (adjacent to the subject site), King Street / TransCanada Highway 101 (adjacent to the subject site), Gervais Street North (adjacent to the subject site), and Queen Street (approximately 25*m* from the nearest part of the subject site), are the most significant roads with potential to impact air quality. The emissions from these roads were calculated using U.S. EPA's Motor Vehicle Emission Simulator (MOVES4) and modelled using AERMOD. The MOVES4 inputs are used by these models to predict the concentrations of NO<sub>2</sub>, Benzene, and PM<sub>2.5</sub> at the subject site and in the surrounding areas. The NPR TRPAP Traffic Assessment Report, from June 2024 was used for an estimate of the traffic flows in 2026 and 2046. The road emissions associated with the train service are represented by the predicted increase in vehicular traffic from 2026 to 2046. MOVES4 was used to estimate vehicle emission rates from 2026, which is conservative as emissions per vehicle are predicted to decrease over time. NO<sub>2</sub>, Benzene, and PM<sub>2.5</sub> were modelled without background levels.

Note: Key Pollutants to air quality impact assessments are; CO, NO<sub>2</sub>, PM<sub>2.5</sub>, Benzene, 1-3 butadiene, formaldehyde, acetaldehyde, acrolein, and benzo(a)pyrene. Oxides of Nitrogen, PM<sub>2.5</sub>, and Benzene have the potential to be the controlling contaminants (**Appendix A.3**).

#### **Emissions from Train Station**

The train will arrive/depart the station at low throttle position. The train throttle position is described by idle and 8 notches. The 1<sup>st</sup> notch being the slow position and the 8<sup>th</sup> notch full throttle. The train is expected to idle at the station for one hour in the southbound direction and 2hrs 20min in the northbound direction. In this report, the analysis of the train will be carried out at notch setting 2, which is understood to be the maximum setting for departing due to speed restrictions and will provide a conservative estimate of the maximum concentration of exhaust emissions from the train station. The station will only accommodate one train at a time. The train emissions are modelled as stationary sources.





It should be noted:

- The train station building will have an emergency natural gas fired generator and comfort heating equipment, the emissions of which have been included in the NO<sub>X</sub>, PM<sub>2.5</sub>, and Benzene emissions.
- The new trains will be built by Siemens Mobility Limited and will meet the latest EPA Tier 4 emission standards.

The predicted concentrations are compared to the Ontario Ambient Air Quality Criteria and the Canadian Ambient Air Quality Standards. For criteria based on hourly limits, the hourly results are reported. Similarly, for criteria based on 24-hour limits, the 24-hour average results are presented, and for annual criteria, the annual average results are provided. The results are organized by contaminant and displayed in **Table 5**.

The results of the dispersion modeling show that the addition of a train and train station in Timmins does not significantly alter the ambient air quality conditions near the proposed station.

Passenger trains are not currently operating on the rail lines at the proposed location. As a result, background conditions based on the 90th percentile of the monitoring station data have been conservatively used to represent the "no build" scenario. The "build" scenario, on the other hand, incorporates the 90th percentile concentrations, modeled emissions from the proposed train station (including idling Tier 4 trains, the emergency natural gas-fired generator, and the air handling units (AHUs)), as well as road emissions associated with the train service to predict the final concentration level

When considering the impact of NO<sub>2</sub>, PM<sub>2.5</sub>, and Benzene on the selected sensitive receptors, the difference between the "No Build" and "Build" scenarios is small and fall within the criteria and standards outlined by the Ontario Ambient Air Quality Criteria (AAQC) and the Environment Canada has the Canadian Ambient Air Quality Standard (CAAQS) in both the "no build" and "build" circumstances.

#### POTENTAL CONSTRUCTION PHASE AIR QUAILTY EFFECTS

Potential air quality impacts associated with the construction stage of the proposed Timmins station are expected to be temporary and localized to the surrounding area. Periodic on-site inspections will be undertaken to confirm the implementation of the mitigation measures and identify corrective actions if required. Visual inspection for dusty conditions in areas of emission sources shall occur daily to ensure mitigation measures are in place and functioning properly. Mitigation measures are outlined in **Table 6** and within **Appendix C**.

#### **GREEN HOUSE GAS EMISSIONS**

An estimate of the greenhouse gas emissions created as part of constructing the proposed Timmins-Porcupine Station was completed. The estimate is based on scaling the floor area of the proposed station to the emissions from constructing the COP26 House, a "business as usual" building, and a building in Thornbury, Ontario, which was analyzed using the building transparency (EC3) model. The proposed Timmins-Porcupine Station greenhouse gas emissions are expected to fall withing the range bound by the above-mentioned buildings, resulting in greenhouse gas emissions of 349.5MgCO<sub>2</sub> to 936.9MgCO<sub>2</sub>. Note: The Timmins-Porcupine Station is in early design development, and as such only a high-level estimate of greenhouse gas emissions is practical.

The cultural meadow on the existing site has carbon stored in the soil, roots, and plants themselves. A very conservative assumption is that all this stored carbon will be lost. Employing the 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories (in particular default factors from table 6.2 and a baseline Soil Organic Carbon value (SOC ref) from table 2.3 and applying these values to equation 2.25) in concert with a 0.8 hectare cultural meadow as currently occupying the site, results in a one-time loss of 68.04 tonnes of carbon.





Regarding greenhouse gas emissions created as part of operating the proposed Timmins-Porcupine Station, anticipated fuel consumption was used to estimate the  $CO_2$  emissions from the reciprocating engines (conservatively, notch 2 for the locomotive engine and rated capacity for the emergency generator) and  $CO_2$  emission factors for natural gas (by volume of natural gas expected to be consumed). The locomotive engine was conservatively operated 200 minutes per day, the station's emergency generator was conservatively operated 64 hours per year (1h per week testing and 1h per month in an actual emergency), and the comfort heating was conservatively assumed to operate one-half of the year at rated capacity. With these assumptions the idling train produces 458 tonnes of  $CO_2$ , the comfort heat 125 tonnes of  $CO_2$ , and the emergency generator 12 tonnes of  $CO_2$ . This is roughly 5.9% of the threshold of being required to report  $CO_2$  emissions in Ontario (https://www.ontario.ca/page/report-greenhouse-gas-ghg-emissions) and 0.00030% of  $CO_2$  emissions from transport in Canada in 2022 (https://publications.gc.ca/collections/collection 2024/eccc/En81-4-2022-1-eng.pdf).

## **RESULTS & CONCLUSIONS**

An Air Quality Impact Assessment was completed to characterize existing conditions and determine the impact of the Project on air quality. Key pollutants for air quality impact assessments include CO, NO<sub>2</sub>, PM<sub>2-5</sub>, Benzene, 1,3-butadiene, formaldehyde, acetaldehyde, acrolein, and benzo(a)pyrene. Among these, oxides of nitrogen, PM<sub>2-5</sub>, and Benzene have the potential to be the controlling contaminants (Appendix A.3). Oxides of nitrogen have the highest emission rate-to-concentration limit ratio, while PM<sub>2-5</sub> and Benzene are characterized by relatively high background concentrations. The air quality impact assessment took into consideration the introduction of Tier 4 technology for the Northlander locomotive fleet.

Background conditions for the 90th percentile concentration data were conservatively used to represent the "no build" scenario, as passenger trains are not currently operating on the rail lines at the proposed location. The "build" scenario was assessed by combining the 90<sup>th</sup> percentile concentrations, the modeled emissions from the proposed train station (including idling Tier 4 trains, the emergency natural gas-fired generator, and the AHUs), and the road emissions associated with the train service. These factors were summed to predict the final concentration levels.

The results of the dispersion modelling demonstrates that the addition of a train, and train station, at the proposed project site in Timmins does not significantly change the ambient air quality conditions in the vicinity of the proposed station. The nine receptors were chosen as representing the most sensitive, closest and hence most conservative points to assess for the analysis. Receptors farther from the station will experience reduced impact from the "build" scenario. When assessing the impact of NO<sub>2</sub>, PM<sub>2.5</sub>, and Benzene on the selected sensitive receptors, the difference between the "No Build" and "Build" scenarios is minimal, with both scenarios falling within the criteria and standards set by the Ontario Ambient Air Quality Criteria (AAQC). Similarly, the Canadian Ambient Air Quality Standard (CAAQS) set by Environment Canada is met under both the "No Build" and "Build" scenarios. Therefore, mitigation is not required and hence this report does not recommend any local air quality impact mitigation.

The GHG emission implications of the project were also assessed by conservatively quantifying the air contaminant and GHG emissions associated with the project for the "build" and "no build" scenarios. Comparison of its results with provincial emission inventories suggests that the project's contribution to these inventories will be very small.

Potential air quality impacts associated with the construction stage of the proposed Timmins station are expected to be temporary and localized to the surrounding area. Periodic on-site inspections will be undertaken to confirm the implementation of the mitigation measures and identify corrective actions if required. Visual inspection for





dusty conditions in areas of emission sources shall occur daily to ensure mitigation measures are in place and functioning properly. A summary of potential effects and mitigation measures are outlined in **Table 6**.





# 1.0 INTRODUCTION

The Ontario Northland Transportation Commission (Ontario Northland) is an agency of the Province of Ontario responsible for providing efficient, safe, and reliable transportation services in Northern Ontario. Current services include inter-community bus passenger and bus parcel delivery services, freight rail services that connect Northeastern Ontario to other markets across Canada and around the world, and passenger rail service on the Polar Bear Express. The Polar Bear Express provides rail service connecting Cochrane to Moosonee and the Communities of the James Bay Coast since 1932. Previously, Ontario Northland operated the Northlander passenger rail service between Toronto and Cochrane, however, this service was discontinued in 2012.

The Government of Ontario has issued direction to Ontario Northland to reinstate passenger rail service between Toronto (Union Station) and Northeastern Ontario via Northlander Passenger Rail (NPR) (the Project).

#### 1.1 O. Reg. 231/08: Transit and Rail Project Assessment Process (TRPAP)

The proposed Timmins-Porcupine Station is subject to an environmental assessment study under *Ontario Regulation 231/08: Transit and Rail Projects Assessment Process* (February 16, 2024). The scope of the TRPAP examines the potential environmental effects associated with the new Timmins-Porcupine Station. In addition, the environmental impact assessment studies also consider the area of land adjacent to the proposed station where a future bus maintenance and storage facility may be built. At the time of preparing this EPR, the decision to build the bus facility was not yet definitive, and therefore an engineering design was not completed. Should the bus facility go forward in the future, the environmental impact assessment studies undertaken as part of the TRPAP will need to be revisited and updated, as required. These updated/additional impact assessment studies will be carried out as part of completing an Environmental Project Report (EPR) Addendum process (as per O. Reg. 231/08), which would also entail Ontario Northland carrying out additional public, stakeholder, and Indigenous Communities consultation. It should be noted that this Air Quality Report will be updated and augmented to include a full air quality modelling assessment of the bus maintenance and storage facility as part of the EPR Addendum process, if this component of the project moves forward in the future.

Refer to **Table 1** for a summary of the project components.





# Table 1: Project Components

Project Component	Approximate Location	Description
Train Station Platform	The train platform is to be located on the east side of the station building.	Train platform material will consist of concrete. Platform features will include tactile warning strips, platform edge, and areas for Accessibility Vehicles to park at the north and south ends of the platform.
Station Building	The station building is surrounded by various station elements, and includes access to Ontario Northland bus bays, municipal bus stop on the street, the train platform, and the parking lot.	<ul> <li>Features in the station building may include:</li> <li>Wicket for Travel Tickets and information;</li> <li>Wicket for parcel drop-off/pick-up;</li> <li>Station waiting area;</li> <li>Station washroom;</li> <li>Breakroom for crews and station staff; and,</li> <li>Staff washroom and utility spaces.</li> </ul>
Station Parking Facilities	Parking facilities will be located on lands adjacent to the proposed Timmins-Porcupine Station. Station building, bus stops, and train platform are in proximity to the parking spaces.	Parking facilities at the station will contain a variety of features designated to accommodate accessibility, taxi stalls, drop off /pick up, general parking, employee parking, etc.
Station Pedestrian Walkway	The station pedestrian walkway is proposed on all sides of the station building. There is access to areas for accessibility, bus stops, and train platform.	Pedestrian walkway is to be built around the station building, providing access to various station elements.
Track Works	Minimal track work to occur near the train station platform. New bumping post will be located east of King Street on the existing tracks.	Minimal track work will be required. Ontario Northland will install new bumping post at the end of the alignment.
Ontario Northland Bus Bays	Bus bays will be situated adjacent to the station building with accessible walkway from station building/platform.	Bus bays to be provided for a seamless connection to Ontario Northland motor coach services.
Bus Storage & Maintenance Facility	A potential Bus Storage & Maintenance Facility would be located east of the station building and platform. The precise location and configuration of facility components will be subject to an engineering design process in the future, if applicable.	The TRPAP has considered the approximate area of land that may be required for the potential future construction of a Bus Storage & Maintenance Facility as part of the technical studies undertaken. Additional impact assessment studies and consultation will be carried out by Ontario Northland in the future and an EPR Addendum prepared, should the facility move forward.





# 1.2 Study Area

The boundaries of the TRPAP study area is depicted in **Figure 1**.



Figure 1: Study Area





# 1.2.1 Timmins-Porcupine Station Site Description

The proposed Timmins-Porcupine Station site in Timmins, Ontario, is located on the southeast side of Falcon Street, to the east of Gervais Street North, and to the north of King Street (TransCanada Highway 101). Highway 101 veers to the north while Falcon Street curves to the east, and as such, these roads intersect and bound the site farther to the northeast. Vehicular access is from Falcon Street.

A mix of forest and low-rise industrial bound the site to all directions with more low-rise residential closer to the site and more forest farther from the site. King Street, Gervais Street North, and Falcon Street are immediately adjacent to the site with Queen Street approximately 25m from the nearest part of the subject site to the nearest section of Queen Street.



Figure 2: Timmins – Porcupine Station Site, Looking South

#### 1.3 Study Objectives

These objectives of the study are as follows:

- *i)* Assess the operational air quality effects of the Project (i.e., the idling train, the station's emergency generator, and the station's comfort heating, as well as road emissions associated with the train service represented by the predicted increase in traffic from 2026 to 2046); identify mitigation measures, as applicable.
- *ii)* Assess the construction phase air quality effects of the Project; identify mitigation measures, as applicable.

#### **1.4 Applicable Legislation / Guidance Documents**

A review of applicable legislation and guidance documents was undertaken and included the following:

- Ontario MECP Guideline A-11: Air Dispersion Modelling Guideline for Ontario,
- Ontario MECP Ambient Air Quality Criteria (AAQC)
- Canada's Air https://ccme.ca/en/air-quality-report, Canadian Ambient Air Quality Standards (CAAQS)





- Ontario MECP D-6 Compatibility between Industrial Facilities
- Ontario MINISTRY OF TRANSPORTATION ENVIRONMENTAL GUIDE FOR ASSESSING AND MITIGATING THE AIR QUALITY IMPACTS AND GREENHOUSE GAS EMISSIONS OF PROVINCIAL TRANSPORTATION PROJECTS

# 1.5 Ontario Ambient Air Quality Criteria (AAQC) and Canadian Ambient Air Quality Standards (CAAQS)

Ambient air quality is assessed through the Ontario Ambient Air Quality Criteria (AAQC) and Environment Canada which has the Canadian Ambient Air Quality Standards (CAAQS). **Table 5**, below, lists concentration standards for chemicals commonly associated with contribution to air pollution in a northern urban / suburban environment.





	Canadian /	Ambient Air (CAAQ	Quality (S)	Standards	Ontario Ambient Air Quality Criteria (AAQC)			
Pollutant	Annual	24 Hour	8 Hour	1 Hour	Annual	24 Hour	8 Hour	1 Hour
Nitrogen Dioxide (NO <sub>2</sub> )	24µg/m³			* 84µg/m³		200µg/m³		400µg/m³
Sulphur Dioxide (SO <sub>2</sub> )	4ppb (10.64µg/m³)			*65ppb (172.9µg/m³)	4ppb (10.64μg/m³)			40ppb (106.4μg/m <sup>3</sup> ) + [67ppb (178.22μg/m <sup>3</sup> ) (10min)]
Carbon Monoxide (CO)							13 <i>ppm</i>	30 <i>ppm</i>
Suspended Particulate Matter < 44um diameter					60µg/m³	120µg/m³		
Particulate Matter smaller than 10 micron (PM <sub>10</sub> )						50µg/m³		
Particulate Matter smaller than 2.5 micron (PM <sub>2.5</sub> )	8.8µg/m³	*27µg/m³				27µg/m³		
Benzene					0.45µg/m³	2.3µg/m³		
1-3 Butadiene					2.0µg/m <sup>3</sup>	10μg/m <sup>3</sup>		
Formaldehyde						65µg/m³		
Acetaldehyde						500μg/m <sup>3</sup>		
Acrolein						0.4µg/m <sup>3</sup>		4.5μg/m³
Benzo(a)pyrene					0.00001µg/m³	0.00005µg/m³		-

#### Table 2: Summary of Ambient Air Quality Criteria / Standards

Concentration (*ppm*) = Concentration ( $mg/m^3$ ) x (0.08205 x T (K)) / Molecular Weigh

\*3-year average of the 98<sup>th</sup> percentile. It should be noted that the U.S. National Ambient Air Quality Standard (NAAQS) was used for 1-hour NO<sub>2</sub>, and PM2.5 NAAQS was used in the AERMOD modeling for this analysis. NAAAQS was selected to ensure alignment with the Canadian Ambient Air Quality Standards' 3-year average of the 98<sup>th</sup> percentile. Due to Ontario's AAQC'sPM2.5 limit, the highest concentrations (rather than the 98<sup>th</sup> percentile) are presented in the results.





#### 1.6 General Assessment Methodology

The following steps were undertaken as part of this assessment:

- Establish background exhaust contaminant levels typical of the subject site based on air quality monitoring station data. This represents the "no build" scenario as there currently no train station or passenger train traffic.
- Carry out air quality modelling (using AERMOD) for all stationary sources, as well as road emissions associated with the train service (e.g., buses, passenger vehicles, on adjacent roads resulting from train service), i.e., assess the "build" scenario.

In order to assess the operational air quality effects associate with the proposed Timmins Station, the key pollutants are CO, NO<sub>2</sub>, PM<sub>44</sub>, PM<sub>10</sub>, PM<sub>2.5</sub>, Benzene, 1,3-butadiene, formaldehyde, acetaldehyde, acrolein, and benzo(a)pyrene. Among these, nitrogen oxides (NO<sub>x</sub>), PM<sub>2.5</sub>, and Benzene have the potential to be the controlling contaminants (see Appendices A.3). Nitrogen oxides have the highest emission rate relative to the concentration limit, while PM<sub>2.5</sub> and Benzene are characterized by relatively high background concentrations.

The AERMOD model was employed to evaluate the impact of emissions from the proposed train idling at the station, the proposed train station's comfort heating equipment, emergency natural gas generator, and road emissions associated with the train service. Further, for NO<sub>2</sub> modelling, the Ozone Limiting Method (OLM) was used (discussed further in **Section 3.1** and **Appendix A.2**).

As described further in **Section 3.3**, the roads within influence distance of the site, Falcon Street (adjacent to the subject site), King Street / TransCanada Highway 101 (adjacent to the subject site), Gervais Street North (adjacent to the subject site), and Queen Street (approximately 25*m* from the nearest part of the subject site), are the most significant roads with potential to impact air quality.





# 2.0 BACKGROUND CONDITIONS AND AIR QUALITY

#### 2.1 Climate

Historical wind data collected at Sudbury Airport and Timmins Airport, comprised of hourly observations of wind speed and direction, was used to determine the wind climate expected at the subject site (**Figure 3**). It should be noted that the Sudbury Airport weather station data is included since the MECP requires Regional Meteorological Data for use with AERMOD.



Figure 3: Historical Wind Data





Meteorological climate information is presented below from the MECP for Station ID 6078285, 48°34'11.000" N, 81°22'36.000" W (Timmins/Victor Power), located approximately 18km to the northwest of the proposed development. According to Canadian Climate Normals for 1991-2020 for this station, the mean annual temperature is estimated at 1.9°C. The warmest month of the year is July with an average temperature of 17.7°C and the coldest month is January with an average -16.4°C temperature. The Timmins Station site recorded an average total annual rainfall of 543.1 mm and an average total annual snowfall of 543.1 mm. Precipitation is distributed throughout the year, with most of the rain occurring between April and October, and with most of the snow occurring between November and March. The maximum average monthly rainfall is 84.8 mm and occurs in September and the maximum average monthly snowfall is 63.8 mm and occurs in December. The Climate Normals are summarized below.

Meteorological Parameters	Jan	Feb	March	April	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Year
Daily Average (°C)	-16.4	-14.4	-7.5	0.9	9.7	15.3	17.7	16.2	11.7	4.5	-3.2	-11.2	1.9
Daily Maximum (°C)	-10.4	-7.6	-0.7	7.2	16.8	22.4	24.4	22.8	17.8	9.1	0.8	-6.5	8.0
Daily Minimum (°C)	-22.3	-21.0	-14.4	-5.3	2.5	8.1	10.9	9.6	5.5	-0.1	-7.1	-15.9	-4.1
Rainfall (mm)	4.0	1.1	14.3	35.3	63.5	77.9	84.8	77.0	81.7	66.8	28.1	8.7	543.1
Snowfall (cm)	59.2	47.9	43.2	25.3	3.1	0.2	0.0	0.0	0.5	13.7	50.8	63.8	307.6
Average Wind Speed (km/h)	11.5	12.5	12.9	13.0	12.4	11.1	10.2	10.0	10.8	11.9	12.4	11.7	11.7
Most Frequent Direction	NW	S	NW	Ν	Ν	S	W	S	S	S	S	S	S
Days with Winds >= 52 km/h	0.17	0.55	0.50	0.58	0.46	0.40	0.05	0.36	0.54	0.42	0.48	0.25	4.8





#### 2.2 Air Quality - Atmospheric Chemistry

#### Nitrogen Monoxide, Nitrogen Dioxide and Ozone

Nitrogen Dioxide  $(NO_2)$  and Ozone  $(O_3)$  are secondary pollutants, which mean they are formed from other pollutants by chemical processes taking place in the atmosphere after emission from their source. Nitrogen dioxide is formed from nitrogen monoxide (NO), which is emitted from combustion processes, such as road vehicles and power plants. This reaction takes place relatively quickly and as such, high nitrogen dioxide concentrations can be found fairly close to the original combustion source. For this reason, nitrogen monoxide and nitrogen dioxide are sometimes grouped together as Nitrogen Oxide (NO<sub>x</sub>) and treated as a primary pollutant.

Ozone forms much more slowly, following complex reactions involving nitrogen oxides, hydrocarbons and oxygen, in the presence of sunlight. Ozone is rapidly destroyed upon contact with nitric oxide, and thus, the ozone concentrations in urban areas tend to be low during the night (no production, only destruction) and highest during the early afternoon (rapid production).

#### Particulate

Particulate matter (PM) includes aerosols, smoke, fumes, dust, fly ash and pollen. Its composition varies with origin, monitoring location, time of year, and atmospheric conditions. Fine particulate matter is primarily formed from chemical reactions in the atmosphere and through fuel combustion (e.g. motor vehicles, power generation, industrial facilities, residential fireplaces and wood stoves, agricultural burning and forest fires). Fine particulate matter can also be formed in the atmosphere through a series of complex chemical reactions and therefore, it is also considered to be a secondary pollutant. During periods of widespread elevated levels of fine particulate, it is estimated that more than 50 per cent of the fine particulate in Ontario comes from the U.S.

#### Carbon Monoxide

There is a direct relationship between traffic and CO impact since exhaust fumes from vehicular traffic are the primary source of CO. Carbon monoxide is a localized gas that dissipates very quickly under normal meteorological conditions. Therefore, CO concentrations decrease substantially as distance from the source increases. The highest CO concentrations are typically found along sidewalk locations directly adjacent to congested roadway intersections.





#### Benzene

Benzene is a volatile organic compound (VOC) that can be found in urban areas due to its use in industrial processes, transportation, and consumer products. It is also a component of gasoline and can be released into the air through fuel combustion. Benzene concentrations can vary depending on several factors such as traffic volume, weather conditions, and proximity to certain industrial facilities.

Since oxides of nitrogen (NO<sub>x</sub>), PM<sub>2.5</sub>, and Benzene have the potential to be the controlling contaminants (as detailed in **Appendix A.3**), the following background concentrations are relevant. Additionally, because the Ozone Limiting Method (OLM) has been used to convert NO<sub>x</sub> concentrations to NO<sub>2</sub> concentrations, background ozone (O<sub>3</sub>) concentrations have also been included.

			Pollutant	t Ozone (O	Ozone O3)			
			Unit	parts per	billion (ppb	)		
2021 fro	m MECP Sul	mmary Report	23.9	36	56	45.17		
			mean	1h 90th	1h max	24h max	90th of 24h av	year
			23.9	35.0	56.0	45.17	32.9	2021
Calcula	Calculated from hourly data			38	64	49.3	34.5	2022
			27.0	41.0	71	48.3	38.3	2023
	3 year averages (ppb			38.0	63.7	47.6	35.2	
	3 year averages (ug/m3)		51.1	76.0	127.3	95.2	70.5	
			Nitrogen D	)ioxide (N	litrogen Di	oxide NO	2)	
			Unit	parts per b	illion (ppb)			
2021 from	MECP Sum	mary Report	5.6	12	56.2	24.3		
			mean	1h 90th	1h max	24h max	24h 90th	year

Calculated from hourly data		5.6	12.0	56.2	24.25	11.0	2021
		6.1	13.8	50.8	29.1	12.8	2022
		5.5	11.9	50.6	23.3	10.2	2023
	3 year averages (ppb)	5.7	12.6	52.5	25.5	11.3	
3 year averages (ug/m3)		11.5	25.1	105.1	51.1	22.7	

	Fine Part							
	Unit	micrograms	per cubic ı	netre				
2021 from MECP Summary Report		mary Report	5.8	11	163	48.8		
			mean	1h 90th	1h max	24h max	90th of 24h av	year
	Calculated from hourly data		5.8	11	163	48.8	9.9	2021
Calculat			5.2	11	45	19.0	8.4	2022
		8.8	14	422	276.2	13.6	2023	
	3 year avera	ges (ug/m3)	6.6	12.0	210.0	114.6	10.6	

Max concentrations in 2023 came from forest fires (<u>https://www.sudbury.com/local-news/special-air-quality-advisory-continues-from-environment-canada-7192990</u>).





#### Benzene

Averaging 2016 2017 2018 2019 2020 2021 Period 0.385 INS Annual 0.328 0.323 N/A N/A 24 hour 90<sup>th</sup> 0.549 0.587 0.556 N/A 0.424 0.419 percentile

Newmarket Federal and Provincial Ambient Air Quality Monitoring Data (unit =  $uq/m^3$ ).

The closest site to Timmins with data available within the past 10 years is Newmarket. The provincial Newmarket site has only annual data and the federal Newmarket site has only 24 hour data. These values are tabulated above.

The latest 3-year average (available) of the annual average is  $0.34ug/m^3$ , and the latest 3 year average (available) of the 90th percentile 24h background Benzene concentration is  $0.47 ug/m^3$ .

#### 2.3 Selection of Monitoring Stations

MECP and National Air Pollution Surveillance (NAPS) monitoring stations in the general vicinity of Timmins Station were reviewed to ensure the most representative background concentrations were selected for the Study Area. **Figure 4** provides the location of the nearest Monitoring Stations. The nearest stations that measure NO<sub>2</sub> and particulate are Sault Ste. Marie, Sudbury, and North Bay, with Sudbury as the closest, while the nearest station that measures Benzene is Newmarket. As such, data from Sudbury was used for NO<sub>2</sub> and particulate while data from Newmarket was used for Benzene. Refer to **Figure 4**.

Additionally, it is important to note that Timmins, Sudbury, and Newmarket have similar land uses, which further supports the applicability and representativeness of this data for the air quality study. All three locations have a variety of housing options, including single-family homes, townhouses, and apartments. Each city has commercial areas with retail stores, offices, and service businesses. Timmins and Sudbury have significant industrial activities, particularly in mining and manufacturing, while Newmarket has light industrial activities and business parks. All three locations prioritize recreational spaces, with parks, trails, and recreational facilities available for residents.

Maximum background concentrations for NO<sub>2</sub>, PM<sub>2.5</sub>, and Benzene exceed either federal or provincial limits, on occasion. The ninetieth percentile concentrations were employed as background concentrations in the estimate of the maximum concentrations at or around the proposed development.











# 3.0 LOCAL AIR QUALITY ASSESSMENT

#### 3.1 Overview - Train Station Operations

The Northlander service will provide one trip per direction, 4-7 days per week. Southbound, the train will depart Timmins Station at approximately 12:00am (midnight). Northbound service will see the train arrive in Timmins by 05:30am.

The train will arrive/depart the station at low throttle position due to speed restrictions. The trains will idle at the station for one hour in the southbound direction and 2hrs 20min in the northbound direction. In this report, the analysis of the train emissions was at a notch setting of 2 even when stationary at the station, which is conservative. For the 24-hour and annual averaging periods, the emissions for the expected idling time per day of 3 hours and 20 minutes was averaged over a 24-hour period.

The US EPA testing of Tier 4 engines require that they perform at the g/hp-h criteria, or better, for a duty cycle that represents normal in-use speeds, loads, and degree of transient activity. <u>https://www.ecfr.gov/current/title-40/chapter-I/subchapter-U/part-1065/subpart-J</u>. Operating from idle to notch 8 is a normal duty cycle with idle the lowest horsepower and notch 8 the highest. As such, the emissions in grams over time at the higher horsepower setting of notch 2 must be greater than the emissions at idle.

For example, notch 2 is estimated as 438 horsepower, neglecting hotelling power requirements. Idle, for the locomotive is approximately 24 horsepower. Heating at maximum, on the coldest days, defines the maximum hotelling energy requirement. Each of the three coach cars has a maximum energy usage of 44kW, and the cab has a maximum energy requirement of 9.1kW, for a total of 141kW (189 horsepower). Idle plus the maximum hotelling power would total 213 horsepower. So, say for PM<sub>2.5</sub>, notch 2 operating at 438 horsepower x 0.03g/hp-h = 13.14g/h, while idle plus the maximum hotelling power would be 213 horsepower x 0.03g/hp-h = 6.39g/h. Therefore notch 2 emissions are conservative for a train idling in the station.

The modelling approach for the emissions from the proposed Timmins-Porcupine Station focusses on NO<sub>X</sub> emissions from heating, comfort, and emergency equipment and emissions from the train's diesel engine. This assumption with respect to heating, comfort, and emergency equipment is based on *section 7.1.1* in Ontario MECP Guideline A-10. AERMOD was used to model these emissions, and the PM<sub>2.5</sub> U.S. National Ambient Air Quality Standard (NAAQS) option was used for particulate behaviour, as it allows for both the highest and the 3-year average of the annual 98th percentile of the hourly and 24-hour average concentrations (**Appendix A.2**). Further, for NO<sub>2</sub> modelling, the Ozone Limiting Method (OLM) was used. The OLM method requires values for the "In Stack NO2/NOX Ratio". The following values were used: Diesel Locomotive = 0.083, Unit Heaters and AHU = 0.100, Generac Generator = 0.187, and Vehicles (AII) = 0.156.

These values are from GUIDANCE FOR NO2 DISPERSION MODELLING IN BRITISH COLUMBIA, (Guidance for NO2 Dispersion Modelling (gov.bc.ca)) was used for the in-stack ratios, page 30. These values are from GUIDANCE FOR NO2 DISPERSION MODELLING IN BRITISH COLUMBIA, (Guidance for NO2 Dispersion Modelling (gov.bc.ca)) were used for the in-stack ratios, page 30.

The new trains/rail cars will meet the latest EPA Tier 4 emission standards. The train diesel engine (Cummins QSK95, 4,400hp) exhaust includes NO<sub>x</sub>, Particulate and Benzene.





Table 3: Locomotive Emission Standards

Yess of edgland manufacture	Thus of standards	Standards (g/bhp-hr)					
fear of original manufacture	Her of standards	NOx	PM	HC	co		
1973-1992 <sup>a</sup>	Tier 0 <sup>b</sup>	8.0	0.22	1.00	5.0		
1993 <sup>a</sup> -2004	Tier 1 <sup>b</sup>	7.4	0.22	0.55	2.2		
2005-2011	Tier 2 <sup>b</sup>	5.5	° 0.10	0.30	1.5		
2012-2014	Tier 3 <sup>c</sup>	5.5	0.10	0.30	1.5		
2015 or later	Tier 4 <sup>d</sup>	1.3	0.03	0.14	1.5		

# Table 1 to § 1033.101-Line-Haul Locomotive Emission Standards

Above are the documented emission rates used in modelling the effect of the proposed Timmins-Porcupine Station on the environment.

Approximately 97% of the Tier 4 locomotive particulate emissions are PM2.5 or smaller, and as such, all of the 0.03 g/hp-hr particulate emissions are considered PM2.5 or smaller.

Benzene emissions from the locomotive were estimated from emission factors from US EPA AP-42 Table 3.3-2.

The train station building will have an emergency natural gas fired generator and comfort heating equipment. The emissions of  $NO_X$ , PM2.5, and Benzene, have been included as station emissions.

#### Benzo[a]pyrene

With regard to benzo[a]pyrene (B(a)P), the following supporting information provides rationale for why levels at the station are considered negligible.

The train will be operating at notch 2, which consumes fuel at approximately 140L/h. We've looked at two scenarios: one with Uncontrolled B(a)P emissions and one with 95% reduction with the Diesel Oxidation Catalyst (DOC) and Diesel Particulate Filter (DPF) that come with Tier 4 engines (note the literature describes this 95% reduction.) Since the idling engine is the station's primary source of PM2.5 and B(a)P, a reasonable estimate of B(a)P concentration at the most affected receptor can be scaled based on the PM2.5 and B(a)P emission rates.

The results are summarized below:



	Max Receptor (#9) 0.554	) PM2.5 (24-h) ug/m3 from Station			
B(a)P emission rate % of PM2.5 emission rate	Estimated 24-h B(a)P Conc (ug/m3)	24-h B(a)P Limit (ug/m3)	Fraction of B(a)P Limit (ug/m3)	% of 24-h B(a)P Limit	
					B(a)P
0.0042732%	2.36737E-05	0.00005	0.47347	47.347%	(Uncontrolled)
0.00021362%	1.18345E-06	0.00005	0.02367	2.367%	B(a)P (Tier 4)

	Max Receptor (#9) 0.079	PM2.5 (annual) ug/m3 from Station			
B(a)P emission rate % of PM2.5 emission rate	Estimated Annual B(a)P Conc (ug/m3)	Annual B(a)P Limit (ug/m3)	Fraction of B(a)P Limit (ug/m3)	% annual of B(a)P Limit	
					B(a)P
0.00427324%	0.000003375857	0.00001	0.33759	33.759%	(Uncontrolled)
0.00021362%	0.000000168759	0.00001	0.01688	1.688%	B(a)P (Tier 4)

Therefore, it can reasonably be concluded that the B(a)P emissions from the idling train are insignificant.

# 3.2 Sensitive Receptors in the Study Area

Two sensitive receptors were located at Pete Landers Park, one in the baseball infield and one in the baseball outfield. Further, a sensitive receptor was located at the Frank P. Whitney Public School. Six sensitive receptors were selected as representative of the residences around the proposed location of the station, as depicted in **Figure 5**. The residential receptors were identified by locating residences that are within 500 m of the proposed station. Contaminant concentrations are similar when in the same vicinity. The nine receptors selected represent the most sensitive and closest locations, providing a conservative basis for the analysis. Receptors located farther from the station will experience a diminished impact from the "build" scenario.







Figure 5: Sensitive Receptors





# **3.3 Road Traffic Data**

The roads within influence distance of the site, Falcon Street (adjacent to the subject site), King Street / TransCanada Highway 101 (adjacent to the subject site), Gervais Street North (adjacent to the subject site), and Queen Street (approximately 25*m* from the nearest part of the subject site), are the most significant roads with potential to impact air quality. The NPR TRPAP Traffic Assessment Report, from June 2024 was used for an estimate of the traffic flows in 2026 and 2046.

According to the 2023 NPR TRPAP Traffic Assessment Report, King Street/(TransCanada Highway 101) has an annual average daily traffic (AADT) of 7,020. The report assumes an increase of 1.5% per year, so the predicted AADT in 2026 would be 7,341 and the predicted AADT in 2046 would be 9,887, an increase of 2,546 vehicles per day. This report also stated that Gervais Street North has an annual average daily traffic (AADT) of 960. Gervais Street North has more traffic than Falcon Street and Queen Street. The traffic flows from Gervais Street North were therefore conservatively used to represent the traffic flows from Falcon Street and Queen Street as well. As the report assumes an increase of 1.5% per year, the predicted AADT in 2026 for Gervais Street would be 1004 and the predicted AADT in 2046 would be 1,352, an increase of 348 vehicles per day.

#### 3.4 Motor Vehicle Emissions Rates

The U.S. EPA's Motor Vehicle Emission Simulator (MOVES) model provides estimates of emission rates from motor vehicles based on a variety of factors such as local meteorology and vehicle fleet composition.

The emissions from the subject roads (as described in **Section 4.0**) were calculated using U.S. EPA's Motor Vehicle Emission Simulator (MOVES4) and modelled using AERMOD. The MOVES4 inputs are used by these models to predict the concentrations of NO<sub>2</sub>, Benzene, and PM<sub>2.5</sub> at the subject site and in the surrounding areas.

The road emissions associated with the train service is represented by the predicted increase in vehicular traffic from 2026 to 2046. In addition, MOVES4 was used to estimate vehicle emission rates from 2026, which is conservative as emissions per vehicle are predicted to decrease over time.

#### 3.5 Air Dispersion Modelling Using AERMOD

Dispersion modelling was completed in accordance with the MECP's "Air Dispersion Modelling Guideline for Ontario" Ver. 3.0 (Guideline A-11), and the US EPA's AERMOD model was employed.

The modelled impact of contaminant emissions is assessed as one-hour, 24-hour, and annual sensitive receptor concentrations. The following dispersion model and pre-processors were used in the assessment:

- AERMOD dispersion model (version 22112); and
- AERMAP surface pre-processor (version 22112).

Climate data is available for Ontario at <u>https://www.ontario.ca/environment-and-energy/map-regional-meteorological-and-terrain-data-air-dispersion-modelling</u>. The data for Ontario is split into 5 regions, with Timmins in the "northern region". This region uses surface station weather data from Sudbury (ID 6068150) and upper air data from White Lake (ID 726320). The data covers a five-year period from 1996 to 2000 and is suitable for AERMET stage 3 processing which allows the wind's approach flow to be customized to suit land use in the vicinity of the subject property. In this report, the forest data set "Sudbury\_forest \_22112" was used and it has been preprocessed by the Ministry with AERMET v22112, thus no stage 3 processing was required.





AERMOD, includes two source types called LINE VOLUME, and RLINE, which are used for modeling roadways. The LINE VOLUME source was used to model the roads.

The parameters for the LINE VOLUME Source were set to:

- Configuration = Adjacent
- Plume Height = 1.7 x Vehicle Height = 2.55m
- Release Height = 0.5 x Plume Height = 1.27m
- Plume Width = 21.0m for highways (four lanes) and 16m for two lane side streets
- Emission Rate (g/s) = Specific for each pollutant (NO<sub>2</sub>, PM<sub>2.5</sub>, and Benzene).

The idling trains were modeled as POINT Sources, located at each end of the train. This allows the maximum concentration to be captured. The train was assumed to be at Notch 2 during idle at the station.

For the site and surrounds, forest makes up most of the surrounds, and as such, rural was chosen for the dispersion coefficients.

From the perspective of the MTO's and the Canadian Transportation Agency's description, sensitive receptors may include outdoor areas and/or indoor spaces in permanent residences, schools, hospitals, daycare centers, and seniors' residences. As such, the railway station itself was not considered for the same structure contamination.

The emission rates from the various stationary sources are summarized below in Table 4.





#### Table 4: Source Summary Table

					1	Source Date	a			<b>Emission Data</b>
Source Identifier	Description	Release Height (m)	Stack Gas Exit Temp (K)	Stack Inside Diameter (m)	Stack Gas Exit Velocity (m/s)	Stack Gas Flow (m <sup>3</sup> /s)	Contaminant	Ontario AAQC (ug/m <sup>3</sup> )	Canadian Ambient Air Quality Standards CAAQS (ug/m <sup>3</sup> )	Emission Rate (See Appendix A.4) (g/s)
Source 1 a	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	NO <sub>2</sub>	400 (lh)	* 84 (lh)	0.158
Source 1 b	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	NO <sub>2</sub>	200 (24h)		0.022
Source 1 c	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	NO <sub>2</sub>		12 (annual)	0.022
Source 1 e	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	particulate <2.5	27 (24h)	* 27 (24h)	0.00051
Source 1 d	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	particulate <2.5		8.8 (annual)	0.00051
Source 1 g	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	benzene	2.3 (24h)		0.00005
Source 1 f	Tier 4 Locomotive Charger using Cummins QSK95	4.40	618.75	0.508	14.82	3.004	benzene	0.45 (annual)		0.00005
Source 2 a	Unit Heaters	4.50	323	0.100	0.78	0.006	NO.	400 (1b)	* 84 (1b)	0.000321
Source 2 b	Unit Heaters	4.50	333	0.100	0.78	0.006	NO <sub>2</sub>	200 (24h)	01(111)	0.000321
Source 2 c	Unit Heaters	4.50	333	0.100	0.78	0.006	NO <sub>2</sub>	, í	12 (annual)	0.000321
Source 2 d	Unit Heaters	4.50	333	0.100	0.78	0.006	particulate <2.5	27 (24h)	* 27 (24h)	0.000056
Source 2 e	Unit Heaters	4.50	333	0.100	0.78	0.006	particulate < 2.5		8.8 (annual)	0.000056
Source 2 f	Unit Heaters	4.50	333	0.100	0.78	0.006	benzene	2.3 (24h)		1.5E-11
Source 2 g	Unit Heaters	4.50	333	0.100	0.78	0.006	benzene	0.45 (annual)		1.5E-11
Source 3 a	Hot Water Heater	4.50	333	0.100	2.02	0.016	NO <sub>2</sub>	400 (24h)	* 84 (lh)	0.000803
Source 3 b	Hot Water Heater	4.50	333	0.100	2.02	0.016	NO <sub>2</sub>	200 (24h)		0.000803
Source 3 c	Hot Water Heater	4.50	333	0.100	2.02	0.016	NO <sub>2</sub>		12 (annual)	0.000803
Source 3 d	Hot Water Heater	4.50	333	0.100	2.02	0.016	particulate <2.5	27 (24h)	* 27 (24h)	0.000141
Source 3 e	Hot Water Heater	4.50	333	0.100	2.02	0.016	particulate < 2.5		8.8 (annual)	0.000141
Source 3 f	Hot Water Heater	4.50	333	0.100	2.02	0.016	benzene	2.3 (24h)		3.7E-11
Source 3 g	Hot Water Heater	4.50	333	0.100	2.02	0.016	benzene	0.45 (annual)		3.7E-11
Source 4 a	Air Handling Units	2.00	333	0.150	1.20	0.021	NO <sub>2</sub>	400 (lh)	* 84 (lh)	0.00107
Source 4 b	Air Handling Units	2.00	333	0.150	1.20	0.021	NO <sub>2</sub>	200 (24h)		0.00107
Source 4 c	Air Handling Units	2.00	333	0.150	1.20	0.021	NO <sub>2</sub>		12 (annual)	0.00107
Source 4 d	Air Handling Units	2.00	333	0.150	1.20	0.021	particulate <2.5	27 (24h)	* 27 (24h)	0.000188
Source 4 e	Air Handling Units	2.00	333	0.150	1.20	0.021	particulate <2.5		8.8 (annual)	0.000188
Source 4 f	Air Handling Units	2.00	333	0.150	1.20	0.021	benzene	2.3 (24h)		4.9E-11
Source 4 g	Air Handling Units	2.00	333	0.150	1.20	0.021	benzene	0.45 (annual)		4.9E-11
Source 5 a	Natural Gas Emergency Generac SG150k W Generator	3.00	323	0.203	18.71	0.606	NO <sub>2</sub>	400 (lh)	* 84 (lh)	0.00838
Source 5 b	Natural Gas Emergency Generac SG150k W Generator	3.00	323	0.203	18.71	0.606	NO <sub>2</sub>	200 (24h)		0.000349
Source 5 c	Natural Gas Emergency Generac SG150k W Generator	3.00	323	0.203	18.71	0.606	NO <sub>2</sub>		12 (annual)	0.000349
Source 5 d	Natural Gas Emergency Generac SG150kW Generator	3.00	323	0.203	18.71	0.606	particulate <2.5	27 (24h)	* 27 (24h)	0.000134
Source 5 e	Natural Gas Emergency Generac SGI50k W Generator	3.00	323	0.203	18.71	0.606	particulate <2.5		8.8 (annual)	0.000134
Source 5 f	Natural Gas Emergency Generac SGI50k W Generator	3.00	323	0.203	18.71	0.606	benzene	2.3 (24h)		0.0000223
Source 5 g	Natural Gas Emergency Generac SG150k W Generator	3.00	323	0.203	18.71	0.606	benzene	0.45 (annual)		0.0000223
* The 3 yes	ar average of the a	nnual 98th p	ercentile of th	e daily 24-ho	ur, or hourly,	average conce	entrations.			1





# 4.0 GREENHOUSE GAS EMISSIONS

At the time of preparing the TRPAP and this study, Timmins-Porcupine Station was in the conceptual design stage, and as such, only a high-level estimate of greenhouse gas emissions is practical at this time. An estimate of the greenhouse gas emissions created to construct the proposed Timmins-Porcupine Station was completed. The estimate is based on scaling the floor area of the proposed station to the emissions from constructing the COP26 (https://circularecology.com/news/low-embodied-carbon-house-designed-with-circular-House economy-principles), a "business as usual" building and a building in Thornbury, Ontario, which was analysed the building transparency (EC3) model using (https://buildingtransparency.org/ec3/buildings/a2bac17d3aa44a7dbb2048a58b875b93?view=uniformat2&sta <u>ge=A5</u>). The "business as usual" building was estimated to produce 1,114 kg  $CO_2/m^2$ , while the COP26 house was estimated to produce 457 kg CO<sub>2</sub>/m<sup>2</sup>. Similarly, the building in Thornbury was estimated to produce 415.6 kg  $CO_2/m^2$ . The proposed Timmins-Porcupine Station is approximately  $841m^2$ . As such, the emissions produced in the construction are likely to fall in the range of 349.5MgCO<sub>2</sub> to 936.9MgCO<sub>2</sub>.

The grass and shrubs on the existing site may be sequestering more carbon dioxide than is emitted from mowing and maintaining the area. Conservatively, B. Jason West and Danelle Haake (https://www.litzsinger.org/research/west-haake.pdf) measured 11.7MgCO<sub>2</sub> per year sequestered by 7.2 acres by a restored tallgrass prairie. The result at this site, is sequestering carbon dioxide at a rate of 3.5MgCO<sub>2</sub> per year, if sequestering is at the rate of a restored Missouri tallgrass prairie.

The cultural meadow on the existing site has carbon stored in the soil, roots, and plants themselves. A very conservative assumption is that all this stored carbon will be lost. Employing the 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories (in particular default factors from table 6.2 and a baseline Soil Organic Carbon value (SOC ref) from table 2.3 and applying these values to equation 2.25) in concert with a 0.8 hectare cultural meadow as currently occupying the site, results in a one time loss of 68.04 tonnes of carbon.

In regard to greenhouse gas emissions created as part of operating the proposed Timmins-Porcupine Station, expected fuel consumption was used to estimate the CO<sub>2</sub> emissions from the reciprocating engines (conservatively, notch 2 for the locomotive engine and full capacity for the emergency generator) and CO<sub>2</sub> emission factors for natural gas (by volume of natural gas expected to be consumed). The locomotive engine was conservatively operated 200 minutes per day, the emergency generator conservatively operated 64 hours per year (1h per week testing and 1h per month in an actual emergency), and the comfort heating was conservatively operated to operate half the year at full capacity. With these assumptions the idling train produces 458 tonnes of CO<sub>2</sub>, the comfort heat 125 tonnes of CO<sub>2</sub>, and the emergency generator 12 tonnes of CO<sub>2</sub>. This is roughly 5.9% of the threshold of being required to report CO<sub>2</sub> emissions in Ontario (https://www.ontario.ca/page/report-greenhouse-gas-ghg-emissions) and 0.00030% of CO<sub>2</sub> emissions from transport in Canada in 2022 (https://publications.gc.ca/collections/collection 2024/eccc/En81-4-2022-1-eng.pdf).





## 5.0 MODELLING RESULTS

Results in this assessment are presented in a worst-case analysis presented in **Table 5** with the observations related to the results presented in **Section 5.1**.

#### 5.1 Worst-Case Analysis

#### 5.1.1 Methodology

Worst-case analysis provides pollutant concentrations predicted under a worst-case condition. The AERMOD dispersion model (version 22112) uses five years of actual meteorological data, running simulations for each hour within that period. The model then identifies the worst-case concentration for each contaminant based on these runs. This approach ensures that the model captures a wide range of meteorological conditions, providing a comprehensive assessment of the air quality impacts. Further, AERMOD processes hourly meteorological data to calculate 24-hour average concentrations. It runs simulations for each hour and then averages the results over a 24-hour period to determine the daily average concentration. For annual averages, AERMOD uses hourly data over the five years to calculate the average concentration. This involves running the model for each hour of each year and then averaging the results to get the annual mean concentration. These methodologies ensure that AERMOD provides accurate and reliable long-term average concentrations for worst-case analysis. Refer to **Appendix A.5** for additional details on the AERMOD modeling utilized in this report.

**Sections 3.1, 3.3, and 3.4** describe conservative emissions from the train station and the road emissions associated with the train service represented by the predicted increase in vehicular traffic from 2026 to 2046, respectively.

The background conditions for the 90<sup>th</sup> percentile data (**Section 2.2**) have been conservatively used to represent the "no build" scenario, as passenger trains are not currently operating on the rail lines at the proposed location. The "build" scenario, on the other hand, includes the 90<sup>th</sup> percentile concentrations, modeled emissions from the proposed train station (such as idling Tier 4 trains, the emergency natural gas-fired generator, and the AHUs), and road emissions associated with the train service. These factors are combined to predict the final cumulative concentration levels.

#### 5.1.2 Results

Predicted concentrations are compared to the Ontario Ambient Air Quality Criteria and the Canadian Ambient Air Quality Standards. For criteria based on hourly limits, the hourly results are reported. Similarly, for criteria based on 24-hour limits, the 24-hour average results are provided, and for annual criteria, the annual average results are presented. The results are organized by contaminant and displayed in **Table 5**.

#### 5.1.2.1 Nitrogen Dioxide

Nitrogen dioxide (NO<sub>2</sub>) has a 1-hour, 24-hour and annual criterion. The background data are the average values from 2021, 2022, and 2023. The 90<sup>th</sup> percentile 1-hour background value is  $25.1ug/m^3$  measured at the Sudbury MECP station. The 90<sup>th</sup> percentile 24-hour background value is  $22.7ug/m^3$  also measured at the Sudbury MECP station. The annual background value is  $11.5ug/m^3$ .

The 24-hour emission rate for the idling train and emergency generator were based on their expected operating time for a 24-hour period. The result of changing the train traffic from no passenger trains per day to a maximum of one train per day, per direction, increases NO<sub>2</sub> concentrations for the three averaging periods. The cumulative





 $NO_2$  concentrations ranged from 11.5% to 14.3% of the strictest criteria / standard at the sensitive receptors for the 24-hour averaging time. It is important to note, background concentration alone is 11.4% of the strictest criteria / standard.

In assessing 1-hour averaging time, the cumulative concentrations (the background, plus the additional concentrations from the station, plus the additional concentrations from the predicted increase in vehicular traffic emissions from 2026 to 2046) ranged from 33.1% to 83.8% of the strictest criteria/standard at the selected sensitive receptors for the strictest 1-hour NO<sub>2</sub> averaging time standard/criteria, while the background concentration alone is 29.9% of the strictest NO<sub>2</sub> criteria/standard. Therefore, the maximum 1-hour NO<sub>2</sub> increases from 29.9% to 83.8% of the strictest criteria/standard for the 1-hour averaging time.

Note: The 1-hour CAAQS limit for  $NO_2$  is based on the 98<sup>th</sup> percentile of the 3-year average of the hourly  $NO_2$  concentrations. As such, the AERMOD result presented represents the 98<sup>th</sup> percentile of the 3-year average.

#### 5.1.2.2 PM2.5

 $PM_{2.5}$  has criteria for both 24-hour and annual limits. The background data used consists of average values from 2021, 2022, and 2023. The 90th percentile 24-hour background value is 12.0 µg/m<sup>3</sup>, measured at the Sudbury MECP station, while the 90th percentile annual background value is 6.6 µg/m<sup>3</sup>, also measured at the Sudbury MECP station.

The result of changing the train traffic from no passenger trains per day to a maximum of one train per day, per direction, is to increase  $PM_{2.5}$  concentrations for both averaging periods. The cumulative  $PM_{2.5}$  concentrations (the background, plus the additional concentrations from the station, plus the additional concentrations from the predicted increase in vehicular traffic emissions from 2026 to 2046) ranged from 44.5% to 46.5% at the selected sensitive receptors for the 24-hour averaging time, while the background concentration alone is 44.4% of the strictest criteria/standard. Therefore, the maximum 24-hour  $PM_{2.5}$  increases from 44.4% to 46.5% of the strictest criteria/standard for the 24-hour averaging time.

The cumulative  $PM_{2.5}$  concentrations ranged from 75.0% to 75.9% at the selected sensitive receptors for the annual averaging time, while the background concentration alone is 75.0% of the strictest criteria/standard. Therefore, the maximum annual  $PM_{2.5}$  increases from 75.0% to 75.9% of the strictest criteria/standard for the annual averaging time.

Note: Due to Ontario's AAQC'sPM2.5 limit, the highest 3-year average concentrations (rather than the 98th percentile) are presented in the results.

#### 5.1.2.3 Benzene

Benzene has a 24-hour and annual criterion. The background data are the average values from 2021, 2022, and 2023. The 90<sup>th</sup> percentile 24-hour background value is  $0.47ug/m^3$  measured at the Newmarket NAPS station. The 90<sup>th</sup> percentile annual background value is  $0.34ug/m^3$  also measured at the Newmarket MECP station.

The result of changing the train traffic from no passenger trains per day to a maximum of one train per day, per direction, is to increase Benzene concentrations for both averaging periods. The cumulative Benzene concentrations (the background, plus the additional concentrations from the station, plus the additional concentrations from the predicted increase in vehicular traffic emissions from 2026 to 2046) ranged from 20.5% to 21.1% of the strictest criteria/standard at the selected sensitive receptors for the 24-hour averaging time, while the background concentration alone is 20.4% of the strictest criteria/standard. Therefore, the maximum 24-hour Benzene increases from 20.4% to 21.1% of the strictest criteria/standard for the 24-hour averaging time.

The cumulative Benzene concentrations ranged from 75.6% to 76.1% of the strictest criteria/standard at the selected sensitive receptors for the annual averaging time, while the background concentration alone is 75.6%





of the strictest criteria/standard. Therefore, the maximum annual Benzene increases from 75.6% to 76.1% of the strictest criteria/standard for the annual averaging time at the worst-case sensitive receptor in "build" scenario.





#### Table 5: Summary of Modelling Results<sup>1</sup>

				Consider Ambient	00th percentile	Reakersund	Max Predicted	Max Predicted		Cumulativa
			Ontario	Air Quality	Background	Background Concentration %	from Proposed	Average Daily Traffic	Cumulative	Cumulative Concentration %
Averaging			AAQC	Standards	Concentration	of strictest	Station	Increase from 2026 to	Concentration	of most strict
Period	Receptor	Contaminant	(ug/m <sup>3</sup> )	CAAQS (ug/m <sup>3</sup> )	(ug/m³)	Criteria/Standard	(ug/m³)	2046 (ug/m <sup>3</sup> )	(ug/m <sup>3</sup> )	Criteria/Standard
1-h	1. Frank P. Krznaric Whitney Public School	NO 2	400	84	25.1	29.9%	2.53	0.137	27.77	33.1%
1-h	2. 524 Queen Street	NO 2	400	84	25.1	29.9%	16.23	0.837	42.17	50.2%
1-n 1-h	3. Pete Landers Park - Inited	NO 2	400	84	25.1	29.9%	23.09	0.493	48.08	53.6%
1-h	5 6164 King Street	NO 2	400	84	25.1	29.9%	17.38	1.369	43.85	52.2%
1-h	6. 101 Gervais Street North	NO 2	400	84	25.1	29.9%	29.86	1.083	56.04	66.7%
1-h	7. 6420 King Street	NO 2	400	84	25.1	29.9%	16.34	0.438	41.88	49.9%
1-h	8. 6235 King Street	NO 2	400	84	25.1	29.9%	29.84	0.856	55.80	66.4%
1-h	9. 6258 King Street	NO 2	400	84	25.1	29.9%	44.48	0.835	70.42	83.8%
24-h	1. Frank P. Krznaric Whitney Public School	NO 2	200		22.7	11.4%	0.22	0.116	23.04	11.5%
24-h	2. 524 Queen Street	NO 2	200		22.7	11.4%	3.58	0.731	27.01	13.5%
24-h	3. Pete Landers Park - infield	NO 2	200		22.7	11.4%	2.18	0.424	25.30	12.7%
24-h	4. Pete Landers Park - outfield	NO 2	200		22.7	11.4%	2.93	0.388	26.02	13.0%
24-h	5. 6164 King Street	NO 2	200		22.7	11.4%	1.97	1.193	25.86	12.9%
24-n	6. 101 Gervals Street North	NO 2	200		22.1	11.4%	2.73	0.944	27.05	13.5%
24-h	8. 6235 King Street	NO 2	200		22.7	11.4%	4.55	0.732	27.98	14.0%
24-h	9. 6258 King Street	NO 2	200		22.7	11.4%	5.11	0.720	28.53	14.3%
appual	1 Frank P. Krzparia Whitnow Public School	NO a		24	11.5	47.9%	0.024	0.026	11 56	49.2%
annual	2. 524 Queen Street	NO 2		24	11.5	47.9%	0.211	0.200	11.91	49.6%
annual	3. Pete Landers Park - infield	NO 2		24	11.5	47.9%	0.367	0.107	11.97	49.9%
annual	4. Pete Landers Park - outfield	NO 2		24	11.5	47.9%	0.507	0.097	12.10	50.4%
annual	5. 6164 King Street	NO 2		24	11.5	47.9%	0.215	0.337	12.05	50.2%
annual	6. 101 Gervais Street North	NO 2		24	11.5	47.9%	0.428	0.260	12.19	50.8%
annual	7. 6420 King Street	NO 2		24	11.5	47.9%	0.504	0.092	12.10	50.4%
annual	8. 6235 King Street	NO 2		24	11.5	47.9%	0.641	0.203	12.34	51.4%
annual	9. 6258 King Street	NO <sub>2</sub>		24	11.5	47.9%	0.841	0.194	12.54	52.2%
24-h	1. Frank P. Krznaric Whitney Public School	particulate <2.5	27	27	12.0	44.4%	0.021	0.002	12.023	44.5%
24-n 24-h	3. Pete Landers Park - infield	particulate <2.5	27	27	12.0	44.4%	0.323	0.008	12.330	45.5%
24-h	4. Pete Landers Park - outfield	particulate <2.5	27	27	12.0	44.4%	0.445	0.007	12.452	46.1%
24-h	5. 6164 King Street	particulate <2.5	27	27	12.0	44.4%	0.242	0.021	12.263	45.4%
24-h	6. 101 Gervais Street North	particulate <2.5	27	27	12.0	44.4%	0.496	0.017	12.513	46.3%
24-n 24-h	7. 6420 King Street	particulate <2.5	27	27	12.0	44.4%	0.340	0.006	12.352	45.7%
24-h	9. 6258 King Street	particulate <2.5	27	27	12.0	44.4%	0.554	0.012	12.566	46.5%
annual	1. Frank P. Krznaric Whitney Public School	particulate <2.5		8.8	6.6	75.0%	0.003	0.001	6.603	75.0%
annual	2. 524 Queen Street	particulate <2.5		8.8	6.6	75.0%	0.025	0.004	6.629	75.3%
annual	3. Pete Landers Park - infield	particulate <2.5		8.8	6.6	75.0%	0.045	0.002	6.647	75.5%
annual	4. Pete Landers Park - outfield	particulate <2.5		8.8	6.6	75.0%	0.066	0.002	6.668	75.8%
annual	5. 6164 King Street	particulate <2.5		8.8	6.6	75.0%	0.027	0.007	6.663	75.4%
annual	7. 6420 King Street	particulate <2.5		8.8	6.6	75.0%	0.057	0.002	6.658	75.7%
annual	8. 6235 King Street	particulate <2.5		8.8	6.6	75.0%	0.072	0.004	6.676	75.9%
annual	9. 6258 King Street	particulate <2.5		8.8	6.6	75.0%	0.079	0.004	6.683	75.9%
24-h	1. Frank P. Krznaric Whitney Public School	benzene	2.3		0.47	20.4%	0.001	0.0002	0.4707	20.5%
24-h	2. 524 Queen Street	benzene	2.3		0.47	20.4%	0.004	0.0014	0.4749	20.6%
24-11 24-h	4 Pete Landers Park - Infled 4 Pete Landers Park - outfield	benzene	2.3		0.47	20.4%	0.005	0.0008	0.4755	20.7%
24-h	5. 6164 King Street	benzene	2.3		0.47	20.4%	0.007	0.0022	0.4796	20.9%
24-h	6. 101 Gervais Street North	benzene	2.3		0.47	20.4%	0.012	0.0018	0.4840	21.0%
24-h	7. 6420 King Street	benzene	2.3		0.47	20.4%	0.006	0.0007	0.4763	20.7%
24-h	8. 0233 KING STREET	benzene	2.3		0.47	20.4%	0.015	0.0014	0.4860	21.1%
000000	1 Fronk D. Krznorio Wilsteer Dublic Satar	henzono	0.45		0.24	75.6%	0.0001	0.0005	0.2402	75.6%
annual	2 524 Queen Street	benzene	0.45		0.34	75.6%	0.0001	0.00005	0.3402	75.6%
annual	3. Pete Landers Park - infield	benzene	0.45		0.34	75.6%	0.000	0.00020	0.3412	75.8%
annual	4. Pete Landers Park - outfield	benzene	0.45		0.34	75.6%	0.00133	0.00018	0.3415	75.9%
annual	5. 6164 King Street	benzene	0.45		0.34	75.6%	0.00079	0.00062	0.3414	75.9%
annual	6. 101 Gervals Street North 7. 6420 King Street	benzene	0.45		0.34	75.6%	0.00153	0.00048	0.3420	76.0%
annual	8. 6235 King Street	benzene	0.45		0.34	75.6%	0.00125	0.00037	0.3414	76.1%
annual	9. 6258 King Street	benzene	0.45		0.34	75.6%	0.00182	0.00036	0.3422	76.0%

<sup>1</sup> Note: The 1-hour CAAQS limit for NO2 is based on the 98th percentile of the 3-year average of the hourly NO2 concentrations. As such, the AERMOD result presented represents the 98th percentile of the 3-year average.





# 6.0 CONCLUSIONS

An Air Quality Impact Assessment was completed to characterize existing conditions and determine the impact of the Project on air quality. Key pollutants for air quality impact assessments include CO, NO<sub>2</sub>, PM<sub>2-5</sub>, Benzene, 1,3-butadiene, formaldehyde, acetaldehyde, acrolein, and benzo(a)pyrene. Among these, oxides of nitrogen, PM<sub>2-5</sub>, and Benzene have the potential to be the controlling contaminants (**Appendix A.3**). Oxides of nitrogen have the highest emission rate-to-concentration limit ratio, while PM<sub>2-5</sub> and Benzene are characterized by relatively high background concentrations. The air quality impact assessment took into consideration the introduction of Tier 4 technology for the Northlander locomotive fleet.

Background conditions for the 90th percentile concentration data were conservatively used to represent the "no build" scenario, as passenger trains are not currently operating on the rail lines at the proposed location. The "build" scenario was assessed by combining the 90<sup>th</sup> percentile concentrations, the modeled emissions from the proposed train station (including idling Tier 4 trains, the emergency natural gas-fired generator, and the AHUs), and the road emissions associated with the train service. These factors were summed to predict the final concentration levels.

The results of the dispersion modelling demonstrates that the addition of a train, and train station, at the proposed project site in Timmins does not significantly change the ambient air quality conditions in the vicinity of the proposed station. The nine receptors were chosen as representing the most sensitive, closest and hence most conservative points to assess for the analysis. Receptors farther from the station will experience reduced impact from the "build" scenario. When assessing the impact of NO<sub>2</sub>, PM<sub>2·5</sub>, and Benzene on the selected sensitive receptors, the difference between the "No Build" and "Build" scenarios is minimal, with both scenarios falling within the criteria and standards set by the Ontario Ambient Air Quality Criteria (AAQC). Similarly, the Canadian Ambient Air Quality Standard (CAAQS) set by Environment Canada is met under both the "No Build" and "Build" scenarios. Therefore, mitigation is not required and hence this report does not recommend any local air quality impact mitigation.

The GHG emission implications of the project were also assessed by conservatively quantifying the air contaminant and GHG emissions associated with the project for the "build" and "no build" scenarios. Comparison of its results with provincial emission inventories suggests that the project's contribution to these inventories will be very small.

Potential air quality impacts associated with the construction stage of the proposed Timmins station are expected to be temporary and localized to the surrounding area. Periodic on-site inspections will be undertaken to confirm the implementation of the mitigation measures and identify corrective actions if required. Visual inspection for dusty conditions in areas of emission sources shall occur daily to ensure mitigation measures are in place and functioning properly. A summary of potential effects and mitigation/monitoring measures are included in **Table 6**.





# 7.0 SUMMARY OF POTENTIAL EFFECTS, MITIGATION AND MONITORING

This section contains the following information:

• **Table 6** summarizes the potential air quality effects, as well as the associated mitigation and monitoring/commitments (as applicable) for the project.

Appendix C contains a Fugitive Dust Best Management Plan.




### Table 6. Summary of Air Quality Mitigation Measures, Monitoring & Commitments

Environmental Component	Potential Effect	Mitigation Measures	Mon
Air Quality - Construction Phase	Construction related air quality effects may pose risks to human health and wellbeing	<ul> <li>Prior to commencement of construction, develop and implement a Construction Air Quality Management Plan (AQMP). The AQMP will:         <ul> <li>Define the Project's air quality impact zone and identify all sensitive receptors within this area.</li> <li>Include explicit commitment to the implementation of all applicable best practices identified in the Environment Canada document, <i>Best Practices for the Reduction of Air Emissions from Construction</i> <i>and Demolition Activities (2005)</i>.</li> </ul> </li> <li>Develop a Communications Protocol and a Complaints Protocol to respond to issues that may develop during construction.</li> </ul>	<ul> <li>Periodic on-site ir implementation c actions if required</li> </ul>
	Fugitive dust may be generated during construction activities that may generate complaints	<ul> <li>Paved/ Unpaved Roads         <ul> <li>Haul routes shall be maintained during operations, to ensure that loose fine material on the haul route surface is minimized.</li> <li>Ensure trucks hauling excavated materials are tarped.</li> <li>Establish efficient traffic patterns to minimize dust generation.</li> <li>A water truck and water supply shall be available to cover the internal haul routes.</li> <li>The truck shall be equipped with a spray bar to deliver the water evenly over the haul route surfaces required to thoroughly wet the surface.</li> <li>The actual watering rate and frequency shall vary, depending on surface moisture conditions and traffic conditions, and shall be triggered whenever the site construction manager observes trucks producing a trailing cloud of dust greater than about 7m. Note: observation by the construction manager is the primary means of dust monitoring.</li> <li>Wet or vacuum-sweeper cleans paved surfaces.</li> <li>Priority should be given to routes that are most susceptible to the above noted causes of high emissions.</li> </ul> </li> <li>Material Handling         <ul> <li>Loading areas shall be maintained during operations, to ensure that loose fine material on the surface is minimized.</li> <li>Ensure trucks hauling excavated materials are tarped when possible.</li> <li>A water truck and water supply shall be available to cover the material handling areas with an adequate water supply.</li> <li>The truck shall be equipped with a spray bar to deliver the water evenly over the ground surface as required to wet the surface.</li> <li>The truck shall be equipped with a spray bar to deliver the water evenly over the ground surface as required to wet the surface.</li> <li>The truck shall be equipped with a spray bar to deliver the site manager observes and traffic conditions, and shall be trig</li></ul></li></ul>	<ul> <li>Visual inspection shall occur daily t functioning prope</li> <li>Response to com         <ul> <li>The Site N</li> <li>Investigat emissions</li> <li>Determin the result</li> <li>If required as required</li> <li>If necessa</li> <li>Respond</li> <li>Documer</li> </ul> </li> </ul>



# nitoring and/or Commitments

inspections will be undertaken to confirm the of the mitigation measures and identify corrective ed.

- n for dusty conditions in areas of emission sources to ensure mitigation measures are in place and perly.
- nplaints Received:
- Manager will:
- ate the site and the circumstances leading to said as of dust driving the complaint, and
- ne if the source of the dust complaint was indeed It of operations
- ed, adjust or modify fugitive dust mitigation systems red to prevent a reoccurrence
- sary, apply additional control measures
- to the complainant(s) in a timely manner
- nt the resulting information in an on-site log





Environmental Component	Potential Effect	Mitigation Measures	Mor
		<ul> <li>Priority should be given to work areas that are most susceptible to the above noted causes of high emissions.</li> <li>Material (Excavation)         <ul> <li>The excavation area shall be equipped with a water spray system capable of supplying water as required to suppress dust emissions. The actual water application rate shall vary, being adjusted as needed to reduce visible dust emission.</li> <li>The spray bars will be triggered whenever the construction manager observes visible dust emissions above the height of the equipment being used or a trail of dust approximately 7m.</li> <li>Masonry and other elements of construction will also be monitored.</li> </ul> </li> <li>Stockpiles         <ul> <li>Disturbance of storage piles shall be minimized where feasible. For active storage piles, the disturbed area shall be minimized to the extent possible.</li> <li>Dry and fine material should be located in areas that minimize their exposure to the prevailing winds.</li> <li>Water may be sprayed onto stockpiles if the site supervisor deems it necessary in order to prevent visible emissions from extending 7m.</li> <li>Wind forecasts shall be monitored regularly during operation to anticipate the need for these measures and allow for next day planning.</li> </ul> </li> <li>General Work Areas         <ul> <li>Water or a suitable wetting agent may be required when material is especially dusty, or when dictated by wind conditions.</li> <li>Good housekeeping practices should be available to cover the work areas.</li> <li>The truck shall be maintained during operations, to ensure that loose fine material on the haul route surface is minimized.</li> <li>A water truck and water supply shall be available to cover the work areas.</li> <li>The truck shall be equipped with a spray bar to deliver the water evenly over the haul route surface as</li></ul></li></ul>	
Air Quality – Operational	Exhaust emissions associated with diesel-powered trains may contribute to local	<ul> <li>When considering the impact of NO<sub>2</sub>, PM<sub>2.5</sub>, and Benzene on the selected sensitive receptors, the difference between the "No Build" and "Build" scenarios is small and falls within the criteria and standards outlined by the Ontario Ambient Air Quality Criteria (AAQC) while Environment Canada has the Canadian Ambient Air Quality Standard (CAAQS) in both the "no build" and "build" circumstances.</li> <li>No mitigation is required to meet criteria.</li> </ul>	<ul> <li>Train engines and maintained to ma</li> <li>Unnecessary train minimized throug</li> <li>Unnecessary non through design a</li> </ul>



nitoring and/or Commitments

nd their emission control equipment will be nanufacturers' specifications. in / engine / propulsion system idling will be

igh technical and operational measures. n-revenue equipment runs will be minimized and planning, wherever possible and reasonable.



Environmental Component	Potential Effect	Mitigation Measures	Moni
	and regional air quality impacts		<ul> <li>Annually, test train produces exhaust compliance with a engine exhaust en</li> </ul>
Air Quality – Future Bus Maintenance and Storage Facility	Construction and operational air quality effects associated with the Future Bus Maintenance and Storage Facility	• N/A (refer to Commitments column)	<ul> <li>If the bus mainten implementation in Assessment to eva operational air qua components.</li> <li>The AQ Assessment facility will be carr undertaken by On stakeholder and Ir consultation.</li> </ul>



### nitoring and/or Commitments

in propulsion and auxiliary power units, which t emissions and ensure that they remain in applicable Transport Canada heavy-duty diesel mission standards.

nance and storage facility proceeds to in the future (post TRPAP), undertake an Air Quality valuate the potential construction related and uality effects of this facility and any ancillary

ent for the future bus maintenance and storage rried out as part of an EPR Addendum to be intario Northland and will include public, Indigenous Communities & Organizations



### 8.0 References

- 1. Ontario Ministry of the Environment, Conservation and Parks (March 2018). Procedure for Preparing an Emission Summary and Dispersion Modelling Report Ver, 4.1 (Guideline A-10).
- 2. Ontario Ministry of the Environment, Conservation and Parks (March 2017). Air Dispersion Modelling Guideline for Ontario Ver. 3,0 (Guideline A-11).
- 3. Ontario Ministry of the Environment, Conservation and Parks (May 2018). Air Contaminants Benchmark List: standards, guidelines, and screening levels for assessing point of impingement concentrations of air contaminants.
- 4. Ontario Ministry of the Environment, Conservation and Parks (November 2020). Ontario's Ambient Air Quality Criteria, https://www.ontario.ca/page/ontarios-ambient-air-quality-criteria.
- 5. Ontario Ministry of the Environment, Conservation and Parks (December 2021). Air Quality in Ontario 2020 Report, https://www.ontario.ca/document/air-quality-ontario-2020-report#.
- 6. City of Toronto. Avoiding the TRAP: Traffic-Related Air Pollution in Toronto and Options for Reducing Exposure. Technical Report. October 2017.





**AERMOD** Information



# Appendix A – AERMOD Appendix

# A.1 Spec Sheets

PPLICATION AND ENGINEE	RING DATA		DEMAND RESPONSE READ
ENGINE SPECIFICATIONS			
General		Cooling System	
Make	Generac	Cooling System Type	Pressurized Closed Recovery
Cylinder #	6	Fan Type	Pusher
Туре	In-line	Fan Speed (BPM)	1 894
Displacement - in <sup>3</sup> (L)	864.71 (14.2)	Ean Diameter - in (mm)	30 (762)
Bore: in (mm)	5.31 (135)		00((02)
Stroke: in (mm)	6.50 (165)	Fuel System	
Compression Ratio	9.5:1		
Intake Air Method	Turbocharged/Aftercooled	- Fuel Time	Natural Cao
Number of Main Bearings	7	Carburator	Down Draft
Connecting Rods	Carbon Steel	- Garburetor	Standard
Cylinder Head	Cast Iron GT250, OHV	- Secondary rulei negulator	Standard
Cylinder Liners	Ductile Iron	Operating Evel Pressure, in H-O (/Pa)	7 - 11 (1 7 - 2 7)
Ignition	Electronic	- Operating ruler ressure- in 1120 (kra)	7-11 (1.7-2.7)
Piston Type	Aluminum		
Crankshaft Type	Ductile Iron	Engine Electrical System	
Lifter Type	Solid		011/00
Intake Valve Material	Special Heat-Resistant Steel	System Voltage	24 VDC
Exhaust Valve Material	High Temperature Steel Alloy	Battery Charger Alternator	57.5 A
Hardened Valve Seats	High Temperature Steel Alloy	Battery Size	See Battery Index 0161970SBY
		Battery Voltage	(2) - 12 VDG
Engine Governing		Ground Polarity	Negative (-)
Governor	Electronic		
Frequency Regulation (Steady State)	±0.25%		
Lubrication System			
Oil Pump	Gear Driven		
Oil Filter Type	Full-Flow with Cartridge		
Engine Oil Capacity: at (1.)	36 2 (24 3)	-	

#### ERNATOR SPECIFICATIONS

Standard Model	K0150124Y21	Standard Excitation	Permanent Magnet
Poles	4	Bearings	Sealed Ball
Field Type	Revolving	Coupling	Direct
nsulation Class - Rotor	н	Prototype Short Circuit Test	Yes
nsulation Class - Stator	н	Voltage Regulator Type	Digital
Total Harmonic Distortion	<5% (3-Phase)	Number of Sensed Phases	All
Telephone Interference Factor (TIF)	< 50	Regulation Accuracy (Steady State)	+0.25%

\$
-
α.
2



# SG150 | 14.2L | 150 kW

INDUSTRIAL SPARK-IGNITED GENERATOR SET

1

EPA Certified Stationary Emergency and Non-Emergency

#### **OPERATING DATA**

DEMAND RESPONSE READY

GENERAC' INDUSTRIAL

#### **POWER RATINGS - NATURAL GAS**

	Standby/Demand	Response	Prime	
Single-Phase 120/240 VAC @1.0pf	150 kW/150 kVA	Amps: 625	135 kW/135 kVA	Amps: 563
Three-Phase 120/208 VAC @0.8pf	150 kW/188 kVA	Amps: 521	135 kW/169 kVA	Amps: 469
Three-Phase 120/240 VAC @0.8pf	150 kW/188 kVA	Amps: 452	135 kW/169 kVA	Amps: 406
Three-Phase 277/480 VAC @0.8pf	150 kW/188 kVA	Amps: 226	135 kW/169 kVA	Amps: 203
Three-Phase 346/600 VAC @0.8pf	150 kW/188 kVA	Amps: 181	135 kW/169 kVA	Amps: 163

#### MOTOR STARTING CAPABILITIES (skVA)

	skVA vs.	Voltage Dip	
277/480 VAC	30%	208/240 VAC	30%
K0150124Y21	326	K0150124Y21	244
K0200124Y21	478	K0200124Y21	361
K0250124Y21	630	K0250124Y21	506
K0300124Y21	790	K0300124Y21	609

### FUEL CONSUMPTION RATES\*

Percent Load	Standby/Demand Response	Prime
25%	840 (23.8)	780 (22.1)
50%	1,380 (39.1)	1,260 (35.7)
75%	1,800 (51.0)	1,680 (47.6)
100%	2,220 (62.9)	2,040 (57.8)

Fuel supply installation must accommodate fuel consumption rates at 100% load.

### COOLING

		Standby/Demand Response	Prime
Air Flow (Fan Air Flow Across Radiator)	scfm (m³/min)	9,162 (259.4)	9,162 (259.4)
Coolant Flow	gpm (Lpm)	90 (340.7)	90 (340.7)
Coolant System Capacity	gal (L)	10.5 (39.7)	10.5 (39.7)
Maximum Operating Ambient Temperature	°F (°C)	122 (50)	122 (50)
Maximum Operating Ambient Temperature (Before Derate)		See Bulletin No. 0199270SSD	See Bulletin No. 0199270SSD
Maximum Additional Radiator Backpressure	in H <sub>2</sub> O (kPa)	0.5 (0.12)	0.5 (0.12)

#### COMBUSTION AIR REQUIREMENTS

	Flow at rated po	wer scfm - (m³/min)	8	Standby/Demand Response 354 (10.0)	Prime 320 (9.1)	· · · · ·	
ENGINE				EXHAUST			
		Standby/Demand Response	Prime			Standby/Demand Response	Prime
Rated Engine Speed	RPM	1,800	1,800	Exhaust Flow (Rated	scfm (m3/min)	1,166 (33.0)	1,043 (29.5)
Horsepower at Rated	hp	232	209	- Output)	(S N) (17).		
kW**				Max. Backpressure	inHG (kPa)	0.75 (2.54)	0.75 (2.54)
Piston Speed	ft/min (m/min)	1,950 (594)	1,950 (594)	(Post Silencer)			//////////////////////////////////////
BMEP	psi (kPa)	118 (814)	106 (732)	Exhaust Temp (Rated	°F (°C)	1.318 (714.4)	1.300 (704.4)
** Refer to "Emissions permitting purposes	Data Sheet" for max	imum bHP for EPA a	nd SCAQMD	Output - Post Silencer)			

Deration – Operational characteristics consider maximum ambient conditions. Derate factors may apply under atypical site conditions. Please contact a Generac Power Systems Industrial Dealer for additional details. All performance ratings in accordance with BS5514 and DIN6271 standards. Standby - See Bulletin 0187500SSB • Demand Response - See Bulletin 10000018250 • Prime - See Bulletin 0187510SSB



GENERAC' INDUSTRIAL

# **STATEMENT OF EXHAUST EMISSIONS** 2016 SPARK-IGNITED, NON-SCAQMD

	Model	Engine	EPA Engine	Fuel	CAT	Comb Cat or	EPA	6	rams/bhp-	hr.	Rated BHP		Fuel Flow
	ANA 5751		Family	0.0000	Req'd*	Separate Cat	Cert #	THC	NOx	CO	RPM	220.0	(lb/hr)
	Q TA25	2.4	GGNXB02.42NN	NG	No	NR	GGNXB02.42NN-005	2.14	2.37	93.95	1800	38.39	16.52
	Q TA25	2.4	GGNXB02.42NL	LPG	No	NR	GGNXB02.42NL-006	1.43	4.38	86.18	1800	43.29	17.59
	SG035	5.4	GGNXB05.42NN	NG	No	NR	GGNXB05.42NN-049	1.60	2.52	95.32	1800	82.10	36.91
	SG035	5.4	GGNXB05.42NL	LPG	No	NR	GGNXB05.42NL-048	1.24	3.45	112.01	1800	82.30	34.60
(E)	SG040	5.4	GGNXB05.42NN	NG	No	NR	GGNXB05.42NN-049	1.60	2.52	95.32	1800	82.10	36.91
SOH	\$G040	5.4	GGNXB05.42NL	LPG	No	NR	GGNXB05.42NL-048	1.24	3.45	112.01	1800	82.30	34.60
Ē	\$G045	5.4	GGNXB05.42NN	NG	No	NR	GGNXB05.42NN-049	1.60	2.52	95.32	1800	82.10	36.91
SS	SG045	5.4	GGNXB05.42NL	LPG	No	NR	GGNXB05.42NL-048	1.24	3.45	112.01	1800	82.30	34.60
:	SG050	5.4	GGNXB05.42NN	NG	No	NR	GGNXB05.42NN-049	1.60	2.52	95.32	1800	82.10	36.91
gine	SG050	5.4	GGNXB05.42NL	LPG	No	NR	GGNXB05.42NL-048	1.24	3.45	112.01	1800	82.30	34.60
E	SG050	6.8	GGNXB06.82NN	NG	No	NR	GGNXB06.82NN-009	1.46	6.5/	30.88	1800	84.90	3/.1/
ited	SG050	6.8	GGNXB06.82NL	LPG	No	NR	GGNXB06.82NL-010	1.86	2.67	172.30	1800	84.66	46.55
lgn	56060	6.8	GGNXBU6.82NN	NG	No	NR	GGNXBUE.82NN-009	1.4/	2.94	/5.88	1800	96.67	38./6
park	SG060	6.8	GGNXB06.82NL	LPG	No	NR	GGNXBU6.82NL-010	1.26	4.23	99.05	1800	96.60	41.20
SIII	560/0	0.8	GGNXBUD.82NN	NG	No	NR	GGNXBU0.82NN+009	1.40	3.00	08.40	1800	109.72	42.3/
Simo	560/0	0.0	CONVDOD DONN	LPG	No	NP	GUNABUO.82NL+010	1.20	3.28	40.00	1800	118.41	31.80
	00000 00000 /DE)	0.0	CCNVD00.02NN	MCADV	No	NID	CONVDOS 02NN-011	0.05	2.80	48.00	1000	127.01	49.02
	SC000 (DF)	0.0	CCMVD00.02NN	MC/LPV	No	ND	CONVDOR COMM-011	1.00	4.24	27.23	1000	120.00	42.00
	SC000	0.0	CCMVD00.02NN	1 PV	No	ND	CCMXD08.02NW-011	0.05	9.00	00.10	1000	127.30	42.00
	50080	8.0	GGNYR08 02NL	LPU	No	NR	GGNYR08.02NL-012	1.00	2.29	71.26	1800	127.40	46.61
	SG100	0.0	GGNYR08 92C1	NG	Ves	Cat Muff	GGNYR08 0201-012	0.17	0.003	0.06	1800	148.00	40.01
	\$6100 (DE)	9.0	GGNXB08 92C1	NG/LPV	Yes	Cat Muff	GGNXB08 92C1-047	0.30	0.400	0.00	1800	133.16	45.36
	\$6100 (DF)	9.0	GGNXB08 92C1	NG/LPI	Yes	Cat Muff	GGNXB08 92C1-047	0.34	0.006	1 10	1800	135.75	45.47
	SG100	90	GGNXB08 92C2	LPG	Yes	Cat Muff	GGNXB08 92C2-029	0.03	0.08	0.13	1800	157.67	53.08
	SG100	9.0	GGNXB08 92C2	1 PI	Yes	Cat Muff	GGNXB08 92G2-029	0.07	0.04	0.30	1800	156 15	54 47
	SG130.150	9.0	GGNXB08.92C3	NG	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	SG130.150 (DF)	9.0	GGNXB08.92C3	NG/LPV	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	SG130.150 (DF)	9.0	GGNXB08.92C3	NG/LPL	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	MG 130,150	9.0	GGNXB08.92C3	NG	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	MG130,150 (DF)	9.0	GGNXB08.92C3	NG/LPV	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	MG130,150 (DF)	9.0	GGNXB08.92C3	NG/LPL	Yes	Cat Muff	GGNXB08.92C3-050	0.10	0.03	0.02	1800	230.30	71.97
	SG130, 150	9.0	GGNXB08.92C4	LPG	Yes	Cat Muff	GGNXB08.92C4-030	0.02	0.57	1.30	1800	230.30	75.43
	SG130, 150	9.0	GGNXB08.92C4	LPL	Yes	Cat Muff	GGNXB08.92C4-030	0.02	0.57	1.30	1800	230.30	75.43
	MG130,150	9.0	GGNXB08.92C4	LPG	Yes	Cat Muff	GGNXB08.92C4-030	0.02	0.57	1.30	1800	230.30	75.43
-	MG130,150	9.0	GGNXB08.92C4	LPL	Yes	Cat Muff	GGNXB08.92C4-030	0.02	0.57	1.30	1800	230.30	75.43
S	SG 150	12.9	GGNXB12.92C2	NG	Yes	Cat Muff	GGNXB12.92C2-031	0.53	0.13	0.53	1800	307.87	107.99
SS (	MG 150	12.9	GGNXB12.92C2	NG	Yes	Cat Muff	GGNXB12.92C2-031	0.53	0.13	0.53	1800	307.87	107.99
gin	SG175	12.9	GGNXB12.92C2	NG	Yes	Cat Muff	GGNXB12.92C2-031	0.53	0.13	0.53	1800	307.87	107.99
Ē	SG200	12.9	GGNXB12.92C2	NG	Yes	Cat Muff	GGNXB12.92C2-031	0.53	0.13	0.53	1800	307.87	107.99
nite	MG200	12.9	GGNXB12.92C2	NG	Yes	Cat Muff	GGNXB12.92C2-031	0.53	0.13	0.53	1800	307.87	107.99
klg	56230	12.9	GGNXB12.92C2	NG	Yes	Cat Mult	GGNXB12.92C2-031	0.38	0.03	0.53	1800	3/9.10	125.30
IEde	56250	12.9	GGNXB12.9202	NG	Yes	Gat Mult	GGNXB12.9202-031	0.38	0.03	0.53	1800	3/9.10	125.3
ge	MG250	12.9	GGNXB12.92G2	NG	Yes	Gat Mutt	GGNXB12.92G2-031	0.38	0.03	0.53	1800	3/9.10	125.3
Lar	562/5	12.9	GGNVD10.0000	NG	Yes	Cat Muff	GGNXB12.92G3-032	0.00	0.00	0.81	2100	477.00	104.20
	50300 MC200	12.9	CCNVD10 0202	MG	Vec	Cat Muff	CCMVD12.3203-032	0.00	0.00	0.01	2150	477.00	104.20
	SG 150 175 200	14.9	CCNVP14 2203	MG	Vec	Cat Muff	GGNVR14 2201-022	0.00	0.00	0.01	1900	304.00	09.54
	MC 150	14.2	CCNVD14.2201	MG	Vec	Cat Muff	CCNVP14.2201-033	0.00	0.05	0.00	1900	204.00	00.54
	MG200	14.2	GGNXB14.2201	NG	Yes	Cat Muff	GGNXB14.2201-033	0.06	0.00	0.39	1800	304.00	98.54
	SG230 250	14.2	GGNXB14 2201	NG	Yes	Cat Muff	GGNXB14 2201-033	0.04	0.00	0.23	1800	374.00	120.84
	MG250	142	GGNXB14.2201	NG	Yes	Cat Muff	GGNXB14 2201-033	0.04	0.02	0.23	1800	374.00	120.84
	SG275.300	14.2	GGNXB14.22C1	NG	Yes	Cat Muff	GGNXB14.22C1-033	0.03	0.03	0.17	1800	460.00	142.8
	MG300	14.2	GGNXB14,22C1	NG	Yes	Cat Muff	GGNXB14.22C1-033	0.03	0.03	0.17	1800	460.00	142.8
	SG350	21.9	GGNXB21.92C1	NG	Yes	Cat Muff	GGNXB21.92C1-034	0.18	0.14	0.82	1800	636.00	201.17
	MG350	21.9	GGNXB21.92C1	NG	Yes	Cat Muff	GGNXB21.92C1-034	0.18	0.14	0.82	1800	636.00	201.17
	SG400	21.9	GGNXB21.92C1	NG	Yes	Cat Muff	GGNXB21.92C1-034	0.18	0.14	0.82	1800	636.00	201.17
	MG400	21.9	GGNXB21.92C1	NG	Yes	Cat Muff	GGNXB21.92C1-034	0.18	0.14	0.82	1800	636.00	201.17
	SG500	25.8	GGNXB25.82C1	NG	Yes	Cat Muff	GGNXB25.82C1-057	0.07	0.07	0.05	1800	777.00	244.4
	MG500	25.8	GGNXR25 82C1	NG	Ves	Cat Muff	GGNXR25 8201-057	0.07	0.07	0.05	1800	777.00	244 40

न WARRANTY & CERTIFICATES उ

\* Three-Way Catalyst (TWC) NR: Not Required DF: Dual Fuel Refer to page 2 for definitions and advisory notes.



Theakston Environmental

Job Information	Technical Data Shee			
Job Name	22307581 Ontario Northland Timmins			
Date	5/10/2024			
Submitted By	Charlotte Paton			
Software Version	12.51			
Unit Tag	AHU-01 Option 2 WW May 10 24			



### Unit Overview

OTHE CARE AREA					
Model Number	Voltage	Design Cooling	AHRI360 Standard Efficiency		A5HRAE 90.1-2022
	V/Hz/Phase	Capacity Btu/hr	EER	IEER	Compliant
DPSH12B	575/60/3	160952	11.9	21.0	A5HRAE 90.1-2022 compliant

Unit

Nodel Number:	DPSH128
Model Type:	Heat Pump
Heat Type:	Gas
Energy Recovery:	None
Application:	Variable Air Volume, Single Zone (Mixed Air or 100% OA)
Controls:	Microtech
Outside Air:	0-100% Economizer with Comparative Enthalpy Control
Altitude:	0 ft
Approval	cETLus

#### Physical

	Dimensions and	d Weight	
Length	Height*	Width	Weight*
101.6 in	85.9 in	73.4 in	2382 lb
	Construct	ion	
Exterior	Insulation and Liners	Air Openin	g Location
		Return	Supply
<sup>p</sup> ainted Galvanized Steel	1" Injected Foam, R-7, Galvanized Steel Liner	Horizontal	Bottom

Electrical			
Unit FLA	MCA	MROPD	SCCR
30.3 A	35.5 A	50 A	10 kAIC
Note:	Use only copper supply wires w terminals must be made with co	ith ampacity based on 75° C cont opper lugs and copper wire.	ductor rating. Connections to

Return/Outside/Exhaust Air		
	Outside Air Option	
Туре	Damper Pressure Drop	Exhaust Air Type
90.1 and California Title 24 Compliant Economizer	0.35 inH <sub>2</sub> 0	Barometric Relief



Filter Section				
		Physical		
Туре	Quantity / Size	Face Area	Face Velocity	Air Pressure Drop
COMBO RACK-2" MERV8 & 4" MERV14 from factory	6 / 18 in x 24 in x 2 in & 6 / 18 in x 24 in x 4 in	18.0 ft²	366.7 ft/min	0.52

DX Cooling Co	il							
				Physical				
Coil Type	Refrigerant Type	Fins per Inch	Rows	Face Are	ea Face V	Velocity	Air Pressure drop	Drain Pan Material
Cu Tube/ Al Fin	R32	15	4	15.4 f	t² 427.	7 ft/min	1.08 inHz0	Stainless Steel
			Cooli	ng Performance				
	Capacity			Indoc	or Air Temperatu	re		Ambient air
Total	Sensible	Moisture	Ente	ering	Leaving			Temperature
Btu/hr	Btu/hr	Removal lb/h	Dry Bulb °F	Wet Bulb °F	Dry Bulb °F	Wet Bulb °F	Dewpoint °F	۴F
160952	160952	0.0	77.7	62.8	54.4	54.2	54.0	85.0

Condensate Connection Size: 3/4 in. Male NPT

		Heating Performance		
Total Capacity	Refrigerant	Indoor Air Temp	Ambient Air	
Btu/hr	Туре	Entering °F	Leaving °F	Temperature °F
86129	R32	64.0	76.1	5.0

in Section				
		Fan		
Туре	Fan Wheel Diameter	Fan Series	Fan Is	solation
SWSI AF	14 in	Series II	N	one
		Performance		
Airflow	Total Static Pressure	Fan Speed	Brake Horsepower	Altitude
6600 CFM	3.9 inH <sub>2</sub> 0	1719 rpm	5.73 HP	0 ft
	Motor			Drive
Туре	Horsepower	Efficiency	FLA	Туре
ECM Motor	6.1	Premium	6.2 A	Direct Drive

s Heat Section							
			Phy	sical			
Airflow	Max Allowab Temp F	ole Burner Rise	Size	Conne	ction (Qty) Size	Heat Ex	changer Material
6600 CFM	60.0	°F	200 MBH	(1) 0.75	in. Female NPT	Stai	nless Steel
			Perfor	mance			
Capacity	Air Temperat	ture Dry Bulb	Air Pr	essure Drop	ssure Drop Gas Pressur		Modulation
Btu/hr	Entering °F	Leavin °F	ve	inH₂O	Minimum inH <sub>2</sub> O	Maximum inH <sub>2</sub> O	
160000	58.4	80.7	•	0.09	5	14	Modulating 10:1 Turndown





Revision: UBXC-TSL (04-24) REV-A Supersedes: UBXC-TSL (02-24) REV-0

# **TECHNICAL SPECIFICATIONS FOR MODEL UBXC**

#### COMMERCIAL/INDUSTRIAL POWER-VENTED HIGH-STATIC BLOWER FAN CONVERTABLE GAS-FIRED UNIT HEATER



#### TABLE OF CONTENTS

Unit Sizes
Features
Factory-Installed Options
Field-Installed Options
Certification
Installation Codes
Technical Data
Clearances
Dimensions
Weights
Hazards of Chlorine
Gas Supply Pressure
Gas Supply Piping
Vent Connections
Heater Throw Distances with Standard Horizontal Louvers
Blower Performance Data for Unit Sizes 30-125 with Direct-Drive Blower Motors
Blower Performance Data for Unit Sizes 150–400
In keeping with our policy of continuous product improvement, we reserve the right

In keeping with our policy of continuous product improvement, we reserve the right to alter, at any time, the design, construction, dimensions, weights, etc., of equipment information shown here.



#### TECHNICAL SPECIFICATIONS—CONTINUED

#### Certification

These unit heaters are listed by Intertek for use in industrial and commercial installations in the United States and Canada.

#### Installation Codes

- These units must be installed in accordance with local building codes. In the absence of local codes, in the United States, the unit must be installed in accordance with the National Fuel Gas Code (ANSI Z223.1, latest edition). A Canadian installation must be in accordance with the Natural Gas and Propane Installation Code (CSA B149, latest edition). This code is available from CSA Information Services, 1-800-463-6727. Local authorities having jurisdiction should be consulted before installation is made to verify local codes and installation procedure requirements.
- Installations in aircraft hangars should be in accordance with the Standard for Aircraft Hangars (ANSI/NFPA No. 409, latest edition). Installations in public garages should be in accordance with the Standard for Parking Structures (ANSI/NFPA No. 88A, latest edition). Installations in repair garages should be in accordance with the Standard for Repair Garages (ANSI/NFPA No. 88B, latest edition). In Canada, installations in aircraft hangars should be in accordance with the standard for Repair Garages (ANSI/NFPA No. 88B, latest edition). In Canada, installations in aircraft hangars should be in accordance with the requirements of the enforcing authorities, and in public garages, in accordance with the CSA B149 code.
- If the heater is being installed in the Commonwealth of Massachusetts, installation must be performed by a licensed plumber or licensed gas fitter.

#### **Technical Data**

Deservator	Unit of			Unit Size	(MBTUh)		
Parameter	Measure	30	45	60	75	100	125
Thermal efficiency	%	8	32	8	32	8	3
	BTUh	30,000	45,000	60,000	75,000	105,000	120,000
Input heating capacity	kW	8.8	13.2	17.6	22.0	30.8	35.2
	BTUh	17,220	25,830	34,440	43,050	61,005	69,720
Output heating capacity, low fire*	kW	5.0	7.6	10.1	12.6	17.9	20.4
0	BTUh	24,600	36,900	49,200	61,500	87,150	99,600
Output heating capacity, high fire-	kW	7.2	10.8	14.4	18.0	25.6	29.2
Gas connection**	in als			1	/2		
Vent connection diameter***	Inch			6	4		
Control, 24V				1	.0		
Full load amps, 115V	amp	3	.7	7	1	13	3.0
Maximum overcurrent protection, 115V <sup>†</sup>		1	15	1	15	3	0
Normal power consumption	watt	2	15	4	47	5:	37
Biashaana aistemaasatuu daa	°F			45	-75		
Discharge air temperature rise	°C		2	7-	-24		
Minimum atomski se s	CFM	304	456	607	759	1076	1230
Minimum air volume	meter <sup>3</sup> /minute	8.6	12.9	17.2	21.5	30.5	34.8
	CFM	506	759	1012	1265	1793	2049
Maximum air volume	meter <sup>3</sup> /minute	14.3	21.5	28.7	35.8	50.8	58.0
	foot <sup>2</sup>	0.	96	1.	25	2.	01
Discharge air opening area	meter <sup>2</sup>	0.	09	0.	12	0.	19
	FPM	316	475	486	607	535	612
Minimum output velocity	meter/minute	96	143	143	179	160	183
	FPM	527	791	810	1012	892	1020
Maximum output velocity	meter/minute	159	239	239	299	267	305
Standard blower motor horsepower	HP	1	/6	1	/3	1	/3
Blower fan size	inch	9	x 6	9	x 6	10 :	x 10
Sound level @ 15 feet	dBa	4	10	40	49	54	55
*ETL ratings for elevations up to 2,000 feet.							
**Size shown is for natural gas or propane of	as connection to a si	ngle-stage g	as valve—no	t supply line	size.		
***Smaller and/or larger vent and combustic	n air pipe diameters i	may be perm	issible.				

<sup>†</sup>MOCP = 2.25 x (largest motor FLA) + smallest motor FLA. Answer is rounded to the next lower standard circuit breaker size.

4

UBXC-TSL (04-24) REV-A



Theakston Environmental

	Unit of		× v.		Unit Size	(MBTUh)	É		
Parameter	Measure	150	175	200	225	250	300	350	400
Thermal efficiency	%		8	13			83		82
lanud baading associate	BTUh	150,000	175,000	200,000	225,000	250,000	300,000	350,000	400,000
Input neating capacity	kW	43.9	51.2	58.6	65.9	73.2	87.8	102.5	117.1
0 + + + × + + + + + + + + + + + + + + +	BTUh	87,150	101,675	116,200	130,725	145,250	174,300	203,350	229,600
Output heating capacity, low fire "	kW	25.5	29.8	34.0	38.3	42.6	51.0	59.6	67.2
Outrant has after an a site, black for \$	BTUh	124,500	145,250	166,000	186,750	207,500	249,000	290,500	328,000
Output neating capacity, high life	kW	36.4	42.5	48.6	54.7	60.8	72.9	85.1	96.0
Gas connection**			1/2		3/4		3	/4	0
Vent connection diameter***	inch		1	5		5		6	
Control, 24V					1	.0			
Full load amps, 115V	amp	5.9	9.6	10.5	12.7	12.7	17.7	27	7.3
Maximum overcurrent protection, 115Vt		15	20	25	30	30	40	6	0
Normal power consumption	watt	230	415	485	675	675	1260	16	35
Discharge statement of state	°F		45-	-75			45-75		50-80
Discharge air temperature rise	°C		7-	-24			7-24		10-27
	CFM	1537	1793	2049	2306	2562	3074	3586	4100
Minimum air volume	meter <sup>3</sup> /minute	43.5	50.8	58.0	65.3	72.5	87.0	101.5	116.1
	CFM	2562	2989	3416	3843	4270	5123	5977	6185
Maximum air volume	meter <sup>3</sup> /minute	72.5	84.6	96.7	108.8	120.9	145.1	169.2	175.1
	foot <sup>2</sup>		2.56		3.51	3.51	4.79	4.	79
Discharge air opening area	meter <sup>2</sup>		0.24		0.33	0.33	0.45	0.	45
	FPM	600	700	800	657	730	642	749	856
Minimum output velocity	meter/minute	183	213	244	200	223	196	228	261
	FPM	1001	1168	1334	1095	1217	1070	1248	1291
Maximum output velocity	meter/minute	305	356	407	334	371	326	380	393
Standard blower motor horsepower	HP	1/4	1/2	1/2	3/4	3/4	1-1/2		2
Blower fan size	inch		12 × 12		15 x 11	15	x 11	15 :	x 15
Sound level @ 15 feet	dBa	51	52	53	56	56	59	61	62
*ETL ratings for elevations up to 2,000 fee	t			50					
**Size shown is for natural gas or propane	gas connection t	a single-	stage gas	valve-no	t supply lin	e size.			
***Smaller and/or larger vent and combus	tion air pipe diame	ters may t	e permiss	sible.					
MOCP = 2.25 × (largest motor ELA) + sm	allest motor FLA	Answeris	rounded to	the next	lower stan	dard circu	it breaker	size	

#### Clearances

Units must be located so that clearances are provided for with regards to combustion air space, inspection, and service and for proper spacing from combustible construction. Clearance to combustibles is defined as the minimum distance from the heater to a surface or object for which it is necessary to ensure that a surface temperature of 90°F (50°C) above the surrounding ambient temperature is not exceeded.

0-125 Minimum Clearar 1 (25) i (152) B (457) 1 (25)	150-400 nce (Inches (mm)) 4 (102) 6 (152) 18 (457)
Minimum Clearar 1 (25) 5 (152) 8 (457) 1 (25)	nce (Inches (mm)) 4 (102) 6 (152) 18 (457)
1 (25) § (152) B (457) 1 (25)	4 (102) 6 (152) 18 (457)
6 (152) B (457) 1 (25)	6 (152) 18 (457)
8 (457)	18 (457)
1 (25)	
1 (20)	2 (51)
1 (25)	1 (25)
8 (457)	18 (457)
ues for variable X (distance Throw Distances with St	e from heater to start of floor coverage) tandard Horizontal Louvers section
	8 (457) ues for variable X (distanc Throw Distances with S

UBXC-TSL (04-24) REV-A



Dimension					Unit Size (MB	TUh)			
(See Graphic	30, 45	60	75	100	125	150, 175	200	225, 250	300, 350, 400
Above)					Inches (mm	1)			
A		-	27 (686)				38-3/16 (970)	í	41 (1041)
В	13-3/4 (349)	16	3-3/4 (425)	24-3/4	4 (629)	20-1/	8 (511)	26-1/8 (664)	34-1/8 (867)
С			13-13/16 (35	1)			23	(584)	
D	10 (254)		13 (330)	21	(533)	16	(406)	22 (559)	30 (762)
E*	17-3/16 (437)	18-	11/16 (475)	24-1/1	6 (611)	30-31/	32 (786)	37-1/32 (941)	41-7/32 (1047)
F	40	)-3/32 (10	018)	48-1/8 (1222)	47-5/8 (1210)	64-3/4	4 (1645)	68-1/8	(1730)
G			25-17/32 (64	9)			40	(1016)	
H**			17-3/8 (441	)			25-11/16 (653	)	27-11/16 (703)
J			1-9/16 (40)				1-13	/32 (36)	
K**			22-1/2 (572	)			24-1/2 (622)		23-1/2 (597)
Ĺ	6-15/32 (	164)	5-15/32 (139)	8-15/32 (215)	7-15/32 (190)	3-29/	32 (99)	5-29/32 (150)	1-13/32 (36)
M	10 (254)	12-	11/16 (322)	19-5/1	6 (491)	13-1/2 (343)	14-9/16 (370)	18-1/16 (459)	22-9/16 (573)
N	6 (152)	8-1	1/16 (221)	15-5/1	6 (389)	8-1/2 (216)	9-9/16 (243)	13-1/16 (332)	17-1/16 (433)
P	3-1/2 (89)	6-	5/16 (160)	9-9/1	6 (243)	5-7/1	6 (138)	9 (229)	11-13/16 (300)
Q			2-21/32 (74	)	1.001 1.0		4-3/16 (106)		4-1/2 (114)
R	5-31/32 (152)	Q	3-5	/16 (84)			6-1/2 (165)		7-5/16 (186)
S	3-5/16 (84)		5-29	/32 (150)			8-3/16 (208)	ų (j. 1	8-1/2 (216)
Т			31 (787)				42	(1067)	
*Varies with mo	tor selection and	d belt adj	ustment for unit s	izes 150-400.					
**Heater suspe	nsion points (3/8		0						1

\*\*Heater suspension points (3/8-16 FEM).

#### Weights

				6		Unit	Size (MB	TUh)					2
Туре	30	45	60	75	100	125	150	175, 200	225	250	300	350	400
	ļ					F	ounds (kg	g)					6
Unit	84 (38)	89 (40)	102 (46)	108 (49)	168 (76)	171 (78)	300 (136)	320 (145)	385 (175)	400 (181)	458 (208)	494 (224)	506 (230)
Shipping	94 (43)	99 (45)	114 (52)	120 (54)	182 (83)	187 (85)	322 (146)	342 (155)	409 (186)	424 (192)	484 (220)	520 (236)	536 (243)

#### Hazards of Chlorine

The presence of chlorine vapors in the combustion air of gas-fired heating equipment presents a potential corrosion hazard for separated-combustion heaters with regard to the combustion air inlet. Chlorine is usually found in the form of freon or degreaser vapors. When chlorine is exposed to flame, it will precipitate from the compound and go into solution with any condensation that is present in the heat exchanger or associated parts. The result is hydrochloric acid, which readily attacks all metals including 300 grade stainless steel. Care should be taken to separate these vapors from the combustion process. This may be done by wise location of the unit vent and combustion air terminals with regard to exhausters or prevailing wind directions. Chlorine is heavier than air. Keep these facts in mind when determining installation location of the heater in relation to building exhaust systems.

UBXC-TSL (04-24) REV-A





Model	Gallon	BTU/h Input Gallon Per	Thermal	Recovery @ 90° Rise	Dimensions	in Inches	Vent	1" W Conne	later ections	T&P	Gas Supply*	Approx. Shipping
Number	Capacity	Hour	Emdency	Hour	A	В	Connection	C	D	E	F	Weight (lbs)
BSS 130	34	130,000	96%	165	48-1/2	22	2 or 3	15-3/4	40-1/2	41	6-3/8	150
BSS 150	34	150,000	94%	190	48-1/2	22	2 or 3	15-3/4	40-1/2	41	6-3/8	150
BTS 130	50	130,000	95%	165	62-3/8	22	2 or 3	15-3/4	54-1/2	55	6-3/8	176
BTS 150	50	150,000	95%	190	63-3/4	22	2 or 3	15-3/4	55-3/4	56-1/4	6-3/8	180
BTS 175	50	175,000	96%	222	63-3/4	22	3	15-3/4	55-3/4	56-1/4	6-3/8	180
BTS 199	50	199,000	96%	253	63-3/4	22	3	15-3/4	55-3/4	56-1/4	6-3/8	180

Available in Propane (LP) gas. Specify when ordering Propane (LP) gas. Models certified for sea level to 7,700 ft. elevation.





#### SUGGESTED SPECIFICATION

(Natural or Propane) gas water heater(s) shall be A. O. Smith Polaris model with storage capacity \_ and input rating of \_ BTUs per hour. Water heater(s) shall have: 1: Tank constructed of 444 stainless steel with submerged combustion chamber. 2: Advanced electronic control w/ LCD display and actual diagnostics. 3: A 3-year limited warranty against tank leaks. Water heater(s) shall meet the thermal efficiency and standby loss requirements of the U.S. Department of Energy and current edition of ASHRAE/IES 90.1 and be design certified by CSA International according to ANSI Z21.10.3-CSA 4.3 standards governing storage tank water heaters.

For Technical Information, call 800-527-1953. A. Q. Smith Corporation reserves the right to make product changes or improvements without prior notice. @ November 2016 A. O. Smith Corporation. All Rights Reserved Page 2 of 2

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A05CG10253



## A.2 Dispersion Modelling

### **Meteorological Conditions**

Climate data is available for Ontario at <u>https://www.ontario.ca/environment-and-energy/map-regional-meteorological-and-terrain-data-air-dispersion-modelling</u>. The data for Ontario is split into 5 regions, with Timmins in the "northern region". This region uses surface station weather data from Sudbury (ID 6068150) and upper air data from White Lake (ID 726320). The data covers a five-year period from 1996 to 2000 and is suitable for AERMET stage 3 processing which allows the wind's approach flow to be customized to suit land use in the vicinity of the subject property. In this report, the forest data set "Sudbury\_forest \_22112" was used and it has been preprocessed by the Ministry with AERMET v22112, thus no stage 3 processing was required.

Figure 1 shows the study area (obtained from Google Earth). Also, a 300m and a 100m radius are shown. For the site and surrounds, mostly forest makes up the surrounds. Rural was chosen for dispersion coefficients.

Sudbury and Timmins Airports wind roses are depicted in Figure 3.

### Area of Modelling Coverage

According to the information from the Ministry of Transportations' Environmental Guide for Assessing and Mitigating the Air Quality Impacts and Greenhouse Gas Emissions of Provincial Transportation Projects the local air quality impacts are assumed to be limited to approximately 500*m* from the transportation facility, in each direction.

Each selected sensitive POI was analysed to determine anticipated concentration levels resulting from the facility's exhaust systems and traffic increases that could be considered due to the proposed station.

### Particulate:

The AERMOD model has 5 options for modeling particulate; TSP, PM<sub>2.5</sub>, PM<sub>10</sub>, PM<sub>2.5</sub> U.S. National Ambient Air Quality Standard (NAAQS), and PM<sub>10</sub> NAAQS. The PM<sub>2.5</sub> NAAQS option was used. This allows for both the highest and the 3-year average of the annual 98th percentile of the daily 24-hour average concentrations. The deposition is based on option 2 (Less than 10% of the particles have a diameter  $\geq$  10 microns). For a Tier 4 locomotive, approximately 97% of the particles in the engine exhaust are sub PM<sub>2.5</sub>. Method 2 above, requires values for "Fine Particle Fraction", set to 1 in this case, and "Mass Mean Particle Diameter" as input. The particle diameter was tested at 0.5, 1.0, 1.5, 2.0, 2.5 microns and the predicted concentrations were the same to 3 decimal places. The values presented in the report represent 2.5 microns. Further, AERMOD does not require input of settling velocity or deposition velocity calculating them internally for the various particle sizes.

### Non-default options within AERMOD modelling:

Non-default options were used for modelling as follows: for Flat Terrain and Method 2 for PM2.5.



### NO<sub>x</sub> to NO<sub>2</sub> Conversion

Currently, AERMOD has three Tiers, with varying degrees of complexity to estimate the  $NO_X$  to  $NO_2$  conversion:

- Tier 1 Total Conversion Method. The simplest method assumes all NO<sub>X</sub> is converted to NO<sub>2</sub> in the atmosphere. This method provides the most conservative estimate of NO<sub>2</sub> concentrations.
- Tier 2 Ambient Ratio Method. This method uses a ratio of  $NO_2$  to  $NO_X$  in the atmosphere to calculate the  $NO_2$  concentrations, based on  $NO_X$ .
- Tier 3 Ozone Limiting Method (OLM) and Plume Volume Molar Ratio Method (PVMRM). These are the most advanced methods, incorporating the ambient ozone (O<sub>3</sub>) concentrations when calculating the resulting concentrations.

Tier 3 OLM was used. This method requires background concentrations for ozone  $(O_3)$  and  $NO_2$ . Typically, this is hourly concentration data for the complete weather data period (5 years), when available. For Timmins this data is not available.

The 90th percentile values for Sudbury were used as representative. These values are shown in Section 2.2 of the report. The 3-year averages from 2021, 2022, and 2023 were used.

The OLM method also requires values for the "In Stack NO<sub>2</sub>/NO<sub>X</sub> Ratio". The following values were used:

- Diesel Locomotive = 0.083,
- Unit Heaters and AHU = 0.100,
- Generac Generator = 0.187,
- Vehicles (All) = 0.156

These values are from GUIDANCE FOR NO<sub>2</sub> DISPERSION MODELLING IN BRITISH COLUMBIA, (Guidance for NO<sub>2</sub> Dispersion Modelling (gov.bc.ca)) was used for the in-stack ratios, page 30.



## A.3 Controlling Contaminants

Key Pollutants to transportation air quality impact assessments are:

CO, NO<sub>2</sub>, PM<sub>44</sub>, PM<sub>10</sub>, PM<sub>2.5</sub>, Benzene, 1-3 butadiene, formaldehyde, acetaldehyde, acrolein, and benzo(a)pyrene.

The AERMOD model was used to evaluate the effects of the emissions from the proposed train, the proposed train station's comfort heating equipment, and the proposed train station's emergency natural gas generator.

Oxides of Nitrogen, PM2.5, and Benzene have the potential to be the controlling contaminants as demonstrated below. Oxides of nitrogen have the highest emission rate to concentration limit of these contaminants, while PM2.5 and Benzene have relatively high background concentrations. The emergency generator and comfort heating equipment are fuelled by natural gas (of small capacity and emitting only a fraction of the emissions coming from the train's engine). Further, the emergency natural gas engine is expected to be tested for 1 hour once per week and conservatively operated in an emergency for 1 hour per month for a total of 64 hours/year. As such, the emissions from the train's engine are the dominant emissions.

Pollutant	E-rate (g/hp-h)	Limit (1h)	Limit (24h)	Limit (annual)	E-rate / 24 h limit	E-rate / Annual limit
NO <sub>2</sub>	Conservatively	84	200	24	0.0065	0.054
	1.3					
PM44 (documented)	0.03		120	60	0.00025 **	
PM <sub>10</sub>	Conservatively		50		0.0006 **	
	0.03					
PM <sub>2.5</sub>	Conservatively		27	8.8	0.0011 **	
	0.03					
CO (documented)	1.5	36,000	14,785.7 *		0.000010	
Benzene (AP 42 - 3.3)	0.00296		2.3		0.0013	
1-3 Butadiene (AP 42 - 3.3)	0.00012		10		0.000012	
Formaldehyde (AP 42 - 3.3)	0.00572		65		0.000088	
Acetaldehyde (AP 42 - 3.3)	0.00244		500		0.0000048	
Acrolein (AP 42 - 3.3)	0.00029		0.4		0.0000725	
Benzo(a)pyrene (AP 42 - 3.3)	0.000000116 ***		0.00005	0.00001	0.0023	0.012

A high emission rate and a low limit results in a large number and identifies the controlling pollutant.

\* calculated based on the 36,000 (1h) limit and the method of averaging period conversion outlined in MECP GUIDELINE A-11 (2017). This calculation, because it is based on the 1-h limit, assumes that the engine is emitting 8760 hours per year.

\*\* Since background concentrations in Ontario are high, combined concentrations are high.

\*\*\* The B(a)P limits are 24h and annual, which allows the emission rate to be averaged over the emission period. For this emission rate, the train was conservatively assumed to emit for 140 minutes,



twice per day (280 minutes), accounting for when the train may be in the station. The train will actually idle at the station for one hour in the southbound direction and 2hrs 20min (summing to 200 minutes) in the northbound direction. The emission rate during the 280-minute period was 0.000000597 g/hp-h and was averaged out over the day.

### A.4 Emission Rate Sample Calculations

Table 1 to § 1033.101-Line-Haul Locomotive Emission Standards

Variation for the state of the	The states deale	St	andards (g	(bhp-hr)	-
Year of original manufacture	Tier of standards	NOX	PM	HC	CO
1973-1992 <sup>a</sup>	Tier 0 <sup>b</sup>	8.0	0.22	1.00	5.0
1993 <sup>a</sup> -2004	Tier 1 <sup>b</sup>	7.4	0.22	0.55	2.2
2005-2011	Tier 2 <sup>b</sup>	5.5	e 0.10	0.30	1.5
2012-2014	Tier 3 <sup>c</sup>	5.5	0.10	0.30	1.5
2015 or later	Tier 4 <sup>d</sup>	1.3	0.03	0.14	1.5

### CURVE FITTING RESULTED IN THE FOLLOWING TABLE:

Approximate	Load (%)	BHP
Notch		
1.9	10	438
2.9	20	875
3.3	25	1094
3.7	30	1313
4.5	40	1750
5.2	50	2188
5.8	60	2626
6.4	70	3063
6.6	75	3282
6.9	80	3501
7.3	90	3938
7.6	100	4376



The train will arrive/depart the station at low throttle position due to speed restrictions. In this report, the analysis of the train's emissions was at a notch setting of 2 even when stationary at the station, which is conservative.

The US EPA testing of Tier 4 engines require that they perform at the g/hp-h criteria, or better, for a duty cycle that represents normal in-use speeds, loads, and degree of transient activity. https://www.ecfr.gov/current/title-40/chapter-I/subchapter-U/part-1065/subpart-J. Operating from idle to notch 8 is a normal duty cycle with idle the lowest horsepower and notch 8 the highest. As such, the emissions in grams over time at the higher horsepower setting of notch 2 must be greater than the emissions at idle.

For example, notch 2 is estimated as 438 horsepower, neglecting hotel power requirements. Idle, for the locomotive is approximately 24 horsepower. Heating at maximum, on the coldest days, defines the maximum hotelling energy requirement. Each of the three coach cars has a maximum energy usage of 44kW, and the cab has a maximum energy requirement of 9.1kW, for a total of 141kW (189 horsepower). Idle plus the maximum hotelling power would total 213 horsepower. So, say for particulate, notch 2 operating at 438 horsepower x 0.03g/hp-h = 13.14g/h, while idle plus the maximum hotelling power would be 213 horsepower x 0.03g/hp-h = 6.39g/h. Therefore notch 2 emissions are conservative for a train idling in the station.

There is empirical data that NOx emissions from the perspective of g/bhp-h, decreases at lower hp. Our empirical data suggests that at 438hp the emission rate would be 0.1042 g/bhp-h, but to be conservative we have uses 0.158 g/bhp-h, as this is the Tier 4 requirement.

Contaminant	(g/hp-h)	g/h	1-h g/s	24-h g/s *					
NOx (Tier 4 Requirement)	1.3	569.40	0.158	0.022	Used f	for the NOx em	ission r	ates	
NOx (Tier 4 reduction at lower HP)	0.8561	374.95	0.1042	0.0145	Not Us	sed for the NO	emissi	on rates	3
PM2.5 (97% of T4 emissions is expected to be smaller than 2.5 <i>um</i>	0.03	13.14	0.00365	0.00051					
Benzene AP-42 3.3	0.00296	1.30	0.00036	0.00005					

\* The Northlander service will provide one trip per direction, 4-7 days per week, travelling overnight in the northern section to allow passengers to maximize daytime at the destination. The train departs Timmins (Porcupine) around midnight, heading south. The train arrives in Timmins (Porcupine) very early next morning, heading north. The train will be idle at the station for one hour in the southbound direction and 2hrs 20min in the northbound direction. The train is therefore expected to idle at the proposed Timmins station for 3 hours and 20 minutes per day. For the 24-hour and annual averaging times, the emission rate is therefore averaged over 24 hours.



<b>Propos</b> Portions	ed Generac SG of the data sheets in	<b>150</b> G the Ap	enerator	nown below:							
SG150 INDUSTRI	AL SPARK-IGNITED GENI Stationary Emergency and Non-Emer	W RATOR SE	т	GEN	ERAC	POWER	RIAL				
					DEMAND RE	SPONSE R	EADY				
Standby Po	ower Rating						_				
150 kW, 18	88 kVA, 60 Hz										
Demand Re 150 kW, 18	esponse Rating 18 kVA, 60 Hz			1.							
135 kW, 16	9 kVA, 60 Hz		- 13		SN-						
ENGINE					EXHAU	JST					
		Star	dby/Demand Response	Prime					Standby	//Demand	Prime
Rated Engir	ne Speed RPM		1,800	1,800	Exhaust	Flow (Rate	d	scfm (m <sup>3</sup> /r	min) 1,166	6 (33.0)	,043 (29.5)
Horsepowe	r at Rated hp		232	209	Max. Ba	ckpressure		inHG (kP	a) 0.75	(2.54)	0.75 (2.54)
Piston Spee	ed ft/min (m/ psi (kP	nin) 1 I)	.950 (594) 1 118 (814)	,950 (594) 106 (732)	(Post Si Exhaust	Temp (Rate	ed	°F (°C)	1,318	(714.4) 1	,300 (704.4)
** Refer to	"Emissions Data Sheet" fo	r maximum	bHP for EPA and	SCAOMD	Output -	Post Silend	cer)		- Data		10
M	odei Engine E	'A Engine Family	Fuel CAT Req'd	* Separate Cat	Cert	#	THC	nams/bnp-nr NOx	CO RPM	BHN H	(lb/hr)
S	G150 12.9 GGI	XB12.92C2	NG Yes	Cat Muff	GGNXB12.9	202-031	0.53	0.13	0.53 1800	307.87	107.99
Load 100%	Rated power EkW 150		Engine BHP 232	NO <sub>x</sub> g/HP.hr 0.130	<b>CO</b> <i>g/HP.hr</i> 0.530	Flow <i>cfm</i> 3930	7	<b>Temp</b> <i>deg F</i> 1318	Flow m3/s 1.85	<b>Temp</b> <i>deg C</i> 714.44	<b>STP flow</b> <i>m3/s</i> 0.55
10070	100		202	0.120	0.000	5750		1010	1100	71111	0.00
										POLE	evation
							sta <mark>ck</mark>	dia. (in	ı) 8	Rela	tive to
		_					stack	dia. (m	a) 0.203	Stack	Exit **
Load	ВНР		CAT Peg'd		CO a/s	Tem	p -	Flow	Velocity	Above	Below
100%	232		ves	0.00838	<b>0.034</b>	50.0	-	0.61	18.71	3.2	2.0
	**	Distanc	e from sourc	e, to pass NO	D <sub>x</sub> limit of	f 500	(b	ased on	stretched st	tring dista	ince)
NOx Emis Max plann	sion during Max Hou	'= is 1h for	0.00838	g/s	nd annual a	weraging	times	: max N(	Dy emission	i 0.00034	a a/s
iviax piariri	led operation in 24 m		testing, there			averaging	y unies	, max no	OX emission	1 0.00034	9 9/5
-		1									
Propos Emission	ed Generac SG factors for natural ga	150 G s recipro	enerator . cating engine	PM2.5 & I s are in lb/MN	Benzene 1Btu from A	P-42 3.2	2				
Max fuel f	low =		107.99	lb/h							
According	g to AP-42 3.2, there	are 1,02	0 Btu/ft3 in na	itural gas and	the fuel ha	s a densi	ty of (	).041 lb/f	t3.		
So,	10	20 Btu /	ft3	x	1	ft3 /	-	24,878	Btu / Ib		
&	107.	99	lb/h x	24,878	Btu / Ib	x	1	1 ,000,000	MMBtu / =	2.69	MMBtu / h
	AP-42 3.2 Lean Bu	rn AP-4	USE 2 3.2 Rich Bu			During Max ho	g jur	Max is fror	planned open testing for	eration 1h in 24	
PM2.5	Engines [lb/MMBtu 0.0000771	ij Eng	nes [lb/MMBt 0.0095	uj MMBtu / h 2.69	lb / h 0.0255	g/s 0.003	2		g / s 0.000134		PM2.5
Benzene	0.00044		0.00158	2.69	0.0042	0.0005	53		2.23E-05		Benzene



Proposed natural gas Boil	er Emi	<u>ssion Rat</u>	e Calculatio	SUO											
These Equations are used to calculate Flu They represent a linear best fit to the bolk been involved with. The equations it most compared to significantly more elaborate i	le gas exit p ers that Thea t boilers with methods.	aroperties. akston has iin 5% when													
Volume Flow Rate (acfm) = 11680 * Inp	urt Capacit	<b>y</b> (MMBtu/hr)													
Mass Flow Rate (lb/hr) = 852.12 * Inpu	t Capacity	(MMBtu/hr)													
To calculate Gas Flow from Mass Flow.	Use the Ic	teal Gas Law													
PV = nRT, where n = mass/MW		So, $P \times V = (n)$	ass/MW) x R x T				Fuel Gas	Fuel Oil	Coal						
	R				MW of E	xhaust Gas (wet)	27.7	29.0	29.0						
		$V = mass \times R$	x T / (MW x P)		MW of E.	xhaust Gas (dry)	29.9	30.4	30.8						
Introd	ucing time					MW of AIR (dry)	28.97								
		V/t = (mass/tir.	me) x R x T / (MW	x P) = Q											
		8314.4×(	r(C) + 273.1	5))		Note that Specific	Volume = $R \times T/l$	(d × MW.							
$Q(m^3/s) = MassFlowRate(i)$	kg/s)×	MM	×101325												
					33480	Specific	Flue Gas	Flue Gas	0						
Description	Percent	Input	Output	Eff	BHP	Volume	Mass Flow	Mass Flow	Volume How	NOX	NOX	femp	Dia	elocity '	Temp
	Load	MMBtu/hr	MMBtu/hr			m3/kg	lb/hr	kg/s	m3/s	Amdd	g/s	С	m	m/s	K
UNIT Heater - Reznor UBXC 60	100%	0.060	0.0492	82%	-	0.987	51.127	0.006	0.006	30	0.000321	60	0.10	0.78	333
Water Heater - AO Smith BTS 150	100%	0.150	0.1425	95%	4	0.987	127.818	0.016	0.016	30	0.000803	60	0.10	2.02	333
AHU - DPSH12B	100%	0.200	0.180	%06	5	0.987	170.424	0.021	0.021	30	0.001070	09	0.15	1.20	333
Description	Percent	Input	PM2.5	PM2.5	PM2.5	Benzene	Benzene	Benzene							
	Load	MMBtu/hr	Ib/MMBtu Input	u/qI	g/s	Ib/MMBtu Input	h/di	s/b							
UNIT Heater - Reznor UBXC 60	100%	0.060	0.0075	0.000447	0.000056	0.0000021	0.0000000012	0.00000000015							
Water Heater - AO Smith BTS 150	100%	0.150	0.0075	0.001118	0.000141	0.0000021	0.00000000029	0.000000000037							
AHI - DPSH12R	100%	0.200	0.0075	0.001490	0.000188	0 000001	0.000000039	0 00000000049							
			2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2												



### A.5 AERMOD Summary Report

Control Pathway - NO2 (1hr)



Pollutant Type	Exponential Decay
NO2 Averaging Time Options	Yes 🕒 No
Hours	Terrain Height Options
Flagpole Receptors Yes No Default Height = 0.00 m	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software CO - 1

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Theakston Environmental

# Control Pathway - NO2 (24hr)

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Dispersion Options Regulatory Default Flat Terrain	Dispersion Coefficient Rural
No Stack-Tip Downwash (NOSTD) Run in Screening Mode Conversion of NOx to NO2 (OLM or PVMRM) No Checks for Non-Sequential Met Data Fast All Sources (FASTALL)	Output Type Concentration Total Deposition (Dry & Wet) Dry Deposition Wet Deposition
Fast Area Sources (FASTAREA)    Optimized Area Source Plume Depletion  Gas Deposition	Plume Depletion Dry Removal Wet Removal Output Warnings
BETA Options: Capped and Horizontal Stack Releases Adjusted Friction Velocity (u*) in AERMET (ADJ_U*) Low Wind Options SCIM (Sampled Chronological Input Model)	No Output Warnings

## Pollutant / Averaging Time / Terrain Options

Pollutant Type	Exponential Decay
NO2 Averaging Time Options	Yes 💽 No
	Terrain Height Options
1 2 3 4 6 8 12 24	Flat Elevated
Month Period I Annual	
Flagpole Receptors	
Yes No	
Default Height = 0.00 m	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h24.isc AERMOD View by Lakes Environmental Software CO - 1



# Control Pathway - PM2.5 (24hr)

**Dispersion Options** 

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		rs	191	U	•

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Dispersion Options Regulatory Default Non-Default Options Flat Terrain	Dispersion Coefficient Rural
No Stack-Tip Downwash (NOSTD) Run in Screening Mode Conversion of NOx to NO2 (OLM or PVMRM) No Checks for Non-Sequential Met Data Fast All Sources (FASTALL)	Output Type Concentration Total Deposition (Dry & Wet) Dry Deposition Wet Deposition
Fast Area Sources (FASTAREA)  Optimized Area Source Plume Depletion Gas Deposition	Plume Depletion Ury Removal Wet Removal
BETA Options:  Capped and Horizontal Stack Releases  Adjusted Friction Velocity (u*) in AERMET (ADJ_U*)  Low Wind Options  SCIM (Sampled Chronological Input Model)  Ignore Urban Night / Daytime Transition (NOURBTRAN)	Output Warnings  No Output Warnings  Non-fatal Warnings for Non-sequential Met Data

### Pollutant / Averaging Time / Terrain Options

Pollutant Type	Exponential Decay
PM2.5	Yes No
Averaging Time Options	
	Terrain Height Options
1 2 3 4 6 8 12 24	Flat Elevated
Month Deriod Deriod Annual	
24-Hour PM-2.5 Non-NAAQS	
24-Hour PM-2.5 NAAQS	
Flagpole Receptors	
Yes No	
Default Height = 0.00 m	

Project File: D:\Projects\2024\24120 Timmins\JANUARY & 2025\PM25h1.isc AERMOD View by Lakes Environmental Software CO - 1



# Control Pathway - Benzene (24hr)

**Dispersion Options** 

AERMOD

Titles D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.i	sc		
Dispersion Options         Regulatory Default         Image: Regulatory Default	Dispersion Coefficient Rural Cutput Type Concentration Total Deposition (Dry & Wet) Dry Deposition Wet Deposition Vet Deposition Dry Removal Wet Removal Output Warnings No Output Warnings No Output Warnings Non-fatal Warnings for Non-sequential Met Data		
Pollutant / Averaging Time / Terrain Options			
Pollutant Type OTHER - BENZENE Averaging Time Options Hours 1 2 3 4 6 8 12 24 Month Period Annual	Exponential Decay  Yes No  Terrain Height Options  Flat Elevated		
Flagpole Receptors			

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software CO - 1

Default Height = 0.00 m



# Source Pathway - Source Inputs - NO2 (1hr)

AERMOD

Source Type	Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation (Optional)	Release Height [m]	Emission Rate [g/s]	Gas Exit Temp. [K]	Gas Exit Velocity [m/s]	Stack Inside Diameter [m]
POINT	STCK1	488178.53 UNIT Heater	5371354.82	281.00	4.50	0.00032	333.00	0.78	0.10
POINT	1STCK2	488180.66 UNIT Heater	5371353.01	281.00	4.50	0.00032	333.00	0.78	0.10
POINT	STCK3	488186.92 Hot Water Heater	5371347.82	281.00	4.50	0.00080	333.00	2.02	0.10
POINT	STCK4	488194.30 AHU	5371350.44	281.00	2.00	0.00107	333.00	1.20	0.15
POINT	STCK5	488191.80 AHU	5371353.01	281.00	2.00	0.00107	333.00	1.20	0.15
POINT	STCK6	488187.79 Generac SG150	5371360.70	281.00	3.00	0.00838	323.00	18.71	0.20
POINT	NETRAIN	488222.33 Train (Cummins QSK	5371358.38 95) NE bound	281.00	4.40	0.15800	618.75	14.82	0.51
POINT	SWTRAIN	488163.01 Train (Cummins QSK	5371287.60 95) SW bound	281.00	4.40	0.15800	618.85	14.82	0.51

Project File: D:\Projects\2024\24120 Timmins\JANUARY & 2025\NO2h1.isc AERMOD View by Lakes Environmental Software

SO1 - 1



Line Volume Sources Source Type: LINE VOLUME Source: SLINE1

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
21.00	0.01135		487682.82	5371245.81	0.00	1.28
			488209.40	5371260.07	0.00	1.28
			488285.16	5371263.82	0.00	1.28
			488333.17	5371269.82	0.00	1.28
			488385.68	5371286.32	0.00	1.28
			488438.19	5371308.82	0.00	1.28
			488487.69	5371338.08	0.00	1.28
			488537.95	5371374.83	0.00	1.28
			488644.47	5371490.35	0.00	1.28

Source Type: LINE VOLUME

Source: SLINEZ	
	_

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00118		488076.72	5371257.50	0.00	1.28
			488072.77	5371821.62	0.00	1.28

# Source Type: LINE VOLUME Source: SLINE3

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]	
16.00	0.00118		488400.62	5371663.72	0.00	1.28	
			488074.16	5371258.79	0.00	1.28	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software

SO1 - 2



Source Type: LINE VOLUME Source: SLINE4

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]	
16.00	0.00118		487675.50	5371347.47	0.00	1.28	
			488155.77	5371360.02	0.00	1.28	

Project File: D:\Projects\2024\24120 Timmins\JANUARY & 2025\NO2h1.isc AERMOD View by Lakes Environmental Software

SO1 - 3

2025-01-11



AERMOD

#### Volume Sources Generated from Line Sources

Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001315	488076.67	5371265.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001316	488076.56	5371281.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001317	488076.44	5371297.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001318	488076.33	5371313.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001319	488076.22	5371329.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001320	488076.11	5371345.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001321	488076.00	5371361.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001322	488075.88	5371377.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001323	488075.77	5371393.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001324	488075.66	5371409.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001325	488075.55	5371425.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001326	488075.44	5371441.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001327	488075.32	5371457.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001328	488075.21	5371473.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001329	488075.10	5371489.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001330	488074.99	5371505.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001331	488074.88	5371521.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001332	488074.76	5371537.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001333	488074.65	5371553.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001334	488074.54	5371569.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001335	488074.43	5371585.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001336	488074.32	5371601.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001337	488074.20	5371617.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001338	488074.09	5371633.49	0.00	1.28	0.00003	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software

SO1 - 4

2025-01-11



AERMOD

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Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001339	488073.98	5371649.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001340	488073.87	5371665.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001341	488073.76	5371681.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001342	488073.64	5371697.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001343	488073.53	5371713.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001344	488073.42	5371729.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001345	488073.31	5371745.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001346	488073.20	5371761.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001347	488073.08	5371777.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001348	488072.97	5371793.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001349	488072.86	5371809.49	0.00	1.28	0.00003	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001350	488395.60	5371657.49	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001351	488385.56	5371645.04	0.00	1.00	0.0000.0	16.00			4.40
		CHARACTER AND CARDEN A RECEIPTION OF A RECE	557 1045.04	0.00	1.20	0.00004	10.00		7.44	1.19
	L0001352	488375.51	5371632.58	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001352 L0001353	488375.51 488365.47	5371632.58 5371620.13	0.00	1.28	0.00004	16.00		7.44 7.44 7.44	1.19 1.19 1.19
	L0001352 L0001353 L0001354	488375.51 488365.47 488355.43	5371632.58 5371620.13 5371607.67	0.00 0.00 0.00 0.00	1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00		7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355	488375.51 488365.47 488355.43 488345.39	5371632.58 5371620.13 5371607.67 5371595.21	0.00 0.00 0.00 0.00 0.00	1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355 L0001356	488375.51 488365.47 488355.43 488345.39 488335.34	5371632.58 5371620.13 5371607.67 5371595.21 5371582.76	0.00 0.00 0.00 0.00 0.00 0.00	1.28 1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355 L0001356 L0001357	488375.51 488365.47 488355.43 488345.39 488335.34 488325.30	5371640.04 5371632.58 5371620.13 5371607.67 5371595.21 5371582.76 5371570.30	0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.28 1.28 1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355 L0001356 L0001357 L0001358	488375.51 488365.47 488355.43 488345.39 488335.34 488325.30 488315.26	5371643.54 5371632.58 5371620.13 5371607.67 5371595.21 5371582.76 5371570.30 5371557.85	0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.28 1.28 1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355 L0001356 L0001357 L0001358 L0001359	488375.51 488365.47 488355.43 488345.39 488335.34 488325.30 488315.26 488305.22	5371632.58 5371632.58 5371620.13 5371607.67 5371595.21 5371582.76 537157.85 537157.85 5371545.39	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.28 1.28 1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.19
	L0001352 L0001353 L0001354 L0001355 L0001356 L0001357 L0001358 L0001359 L0001360	488375.51 488365.47 488355.43 488355.43 488355.39 488335.34 488325.30 488315.26 488305.22 488295.18	5371632.58 5371632.58 5371620.13 5371607.67 5371595.21 5371595.21 5371570.30 5371557.85 5371557.85 5371545.39 5371532.93	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.28 1.28 1.28 1.28 1.28 1.28 1.28 1.28	0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004 0.00004	16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00		7.44 7.44 7.44 7.44 7.44 7.44 7.44 7.44	1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.19

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SO1 - 5



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height ſmſ	Emission Rate [ɑ/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001362	488275.09	5371508.02	0.00	1.28	0.00004	16.00	11	7.44	1.19
	L0001363	488265.05	5371495.56	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001364	488255.01	5371483.11	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001365	488244.97	5371470.65	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001366	488234.92	5371458.20	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001367	488224.88	5371445.74	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001368	488214.84	5371433.28	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001369	488204.80	5371420.83	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001370	488194.75	5371408.37	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001371	488184.71	5371395.92	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001372	488174.67	5371383.46	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001373	488164.63	5371371.00	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001374	488154.59	5371358.55	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001375	488144.54	5371346.09	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001376	488134.50	5371333.63	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001377	488124.46	5371321.18	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001378	488114.42	5371308.72	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001379	488104.37	5371296.27	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001380	488094.33	5371283.81	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001381	488084.29	5371271.35	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001382	488074.25	5371258.90	0.00	1.28	0.00004	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001383	487683.50	5371347.67	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001384	487699.49	5371348.09	0.00	1.28	0.00004	16.00		7.44	1.19

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SO1 - 6



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001385	487715.49	5371348.51	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001386	487731.48	5371348.93	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001387	487747.48	5371349.35	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001388	487763.47	5371349.76	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001389	487779.47	5371350.18	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001390	487795.46	5371350.60	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001391	487811.46	5371351.02	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001392	487827.45	5371351.44	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001393	487843.45	5371351.86	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001394	487859.44	5371352.27	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001395	487875.43	5371352.69	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001396	487891.43	5371353.11	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001397	487907.42	5371353.53	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001398	487923.42	5371353.95	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001399	487939.41	5371354.36	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001400	487955.41	5371354.78	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001401	487971.40	5371355.20	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001402	487987.40	5371355.62	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001403	488003.39	5371356.04	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001404	488019.38	5371356.46	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001405	488035.38	5371356.87	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001406	488051.37	5371357.29	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001407	488067.37	5371357.71	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001408	488083.36	5371358.13	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001409	488099.36	5371358.55	0.00	1.28	0.00004	16.00		7.44	1.19

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SO1 - 7



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001410	488115.35	5371358.96	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001411	488131.35	5371359.38	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001412	488147.34	5371359.80	0.00	1.28	0.00004	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001413	487693.32	5371246.10	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001414	487714.31	5371246.67	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001415	487735.30	5371247.24	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001416	487756.29	5371247.80	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001417	487777.29	5371248.37	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001418	487798.28	5371248.94	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001419	487819.27	5371249.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001420	487840.26	5371250.08	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001421	487861.26	5371250.64	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001422	487882.25	5371251.21	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001423	487903.24	5371251.78	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001424	487924.23	5371252.35	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001425	487945.22	5371252.92	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001426	487966.22	5371253.48	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001427	487987.21	5371254.05	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001428	488008.20	5371254.62	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001429	488029.19	5371255.19	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001430	488050.19	5371255.76	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001431	488071.18	5371256.33	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001432	488092.17	5371256.89	0.00	1.28	0.00023	21.00		9.77	1.19

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SO1 - 8



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001433	488113.16	5371257.46	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001434	488134.16	5371258.03	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001435	488155.15	5371258.60	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001436	488176.14	5371259.17	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001437	488197.13	5371259.73	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001438	488218.12	5371260.50	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001439	488239.09	5371261.54	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001440	488260.07	5371262.57	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001441	488281.04	5371263.61	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001442	488301.91	5371265.91	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001443	488322.74	5371268.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001444	488343.18	5371272.96	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001445	488363.21	5371279.26	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001446	488383.25	5371285.56	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001447	488402.64	5371293.59	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001448	488421.94	5371301.86	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001449	488441.05	5371310.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001450	488459.13	5371321.20	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001451	488477.21	5371331.88	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001452	488494.81	5371343.28	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001453	488511.76	5371355.68	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001454	488528.71	5371368.08	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001455	488544.43	5371381.86	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001456	488558.66	5371397.30	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001457	488572.90	5371412.74	0.00	1.28	0.00023	21.00		9.77	1.19

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SO1 - 9



										AERMO
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE1	L0001458	488587.14	5371428.17	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001459	488601.37	5371443.61	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001460	488615.61	5371459.05	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001461	488629.84	5371474.49	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001462	488644.08	5371489.93	0.00	1.28	0.00023	21.00		9.77	1.19

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SO1 - 10


## Source Pathway - Source Inputs NO2 (24hr & Annual)

Point Sources									
Source Type	Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation (Optional)	Release Height [m]	Emission Rate [g/s]	Gas Exit Temp. [K]	Gas Exit Velocity [m/s]	Stack Inside Diameter [m]
POINT	STCK1	488178.53 UNIT Heater	5371354.82	281.00	4.50	0.00032	333.00	0.78	0.10
POINT	1STCK2	488180.66 UNIT Heater	5371353.01	281.00	4.50	0.00032	333.00	0.78	0.10
POINT	STCK3	488186.92 Hot Water Heater	5371347.82	281.00	4.50	0.00080	333.00	2.02	0.10
POINT	STCK4	488194.30 AHU	5371350.44	281.00	2.00	0.00107	333.00	1.20	0.15
POINT	STCK5	488191.80 AHU	5371353.01	281.00	2.00	0.00107	333.00	1.20	0.15
POINT	STCK6	488187.79 Generac SG150	5371360.70	281.00	3.00	0.00035	323.00	18.71	0.20
POINT	NETRAIN	488222.33 Train (Cummins QSK	5371358.38 95) NE bound	281.00	4.40	0.02197	618.75	14.82	0.51
POINT	SWTRAIN	488163.01 Train (Cummins QSK	5371287.60 95) SW bound	281.00	4.40	0.02197	618.85	14.82	0.51

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SO1 - 1

2025-01-11



Line Volume Sources Source Type: LINE VOLUME

Source: SLINE1

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
21.00	0.01135		487682.82	5371245.81	0.00	1.28
			488209.40	5371260.07	0.00	1.28
			488285.16	5371263.82	0.00	1.28
			488333.17	5371269.82	0.00	1.28
			488385.68	5371286.32	0.00	1.28
			488438.19	5371308.82	0.00	1.28
			488487.69	5371338.08	0.00	1.28
			488537.95	5371374.83	0.00	1.28
			488644.47	5371490.35	0.00	1.28

Source Type: LINE VOLUME

Sou	ce.	SLINE2	
			-

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00118		488076.72	5371257.50	0.00	1.28
			488072.77	5371821.62	0.00	1.28

#### Source Type: LINE VOLUME Source: SLINE3

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00118		488400.62	5371663.72	0.00	1.28
			488074.16	5371258.79	0.00	1.28

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SO1 - 2



Source Type: LINE VOLUME Source: SLINE4

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00118		487675.50	5371347.47	0.00	1.28
			488155.77	5371360.02	0.00	1.28

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h24.isc AERMOD View by Lakes Environmental Software

SO1 - 3

2025-01-11



#### Volume Sources Generated from Line Sources

Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001315	488076.67	5371265.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001316	488076.56	5371281.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001317	488076.44	5371297.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001318	488076.33	5371313.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001319	488076.22	5371329.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001320	488076.11	5371345.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001321	488076.00	5371361.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001322	488075.88	5371377.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001323	488075.77	5371393.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001324	488075.66	5371409.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001325	488075.55	5371425.50	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001326	488075.44	5371441.49	0.00	1.28	0.00003	16.00		7.44	1.19
5	L0001327	488075.32	5371457.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001328	488075.21	5371473.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001329	488075.10	5371489.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001330	488074.99	5371505.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001331	488074.88	5371521.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001332	488074.76	5371537.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001333	488074.65	5371553.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001334	488074.54	5371569.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001335	488074.43	5371585.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001336	488074.32	5371601.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001337	488074.20	5371617.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001338	488074.09	5371633.49	0.00	1.28	0.00003	16.00		7.44	1.19

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SO1 - 4

2025-01-11



										AERM
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001339	488073.98	5371649.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001340	488073.87	5371665.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001341	488073.76	5371681.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001342	488073.64	5371697.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001343	488073.53	5371713.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001344	488073.42	5371729.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001345	488073.31	5371745.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001346	488073.20	5371761.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001347	488073.08	5371777.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001348	488072.97	5371793.49	0.00	1.28	0.00003	16.00		7.44	1.19
	L0001349	488072.86	5371809.49	0.00	1.28	0.00003	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001350	488395.60	5371657.49	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001351	488385.56	5371645.04	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001352	488375.51	5371632.58	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001353	488365.47	5371620.13	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001354	488355.43	5371607.67	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001355	488345.39	5371595.21	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001356	488335.34	5371582.76	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001357	488325.30	5371570.30	0.00	1.28	0.00004	16.00		7.44	1.19
	100 0.000 0.000 0.000 0.000	100015.00	E074EE7 0E	0.00	1 28	0.00004	16.00		7.44	1.19
	L0001358	488315.26	557 1557.65	0.00	1.20					
	L0001358 L0001359	488315.26	5371557.85	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001358 L0001359 L0001360	488315.26 488305.22 488295.18	5371537.65 5371545.39 5371532.93	0.00	1.28	0.00004	16.00 16.00		7.44 7.44	1.19 1.19

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SO1 - 5



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height ſmſ	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001362	488275.09	5371508.02	0.00	1.28	0.00004	16.00	11	7.44	1.19
	L0001363	488265.05	5371495.56	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001364	488255.01	5371483.11	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001365	488244.97	5371470.65	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001366	488234.92	5371458.20	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001367	488224.88	5371445.74	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001368	488214.84	5371433.28	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001369	488204.80	5371420.83	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001370	488194.75	5371408.37	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001371	488184.71	5371395.92	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001372	488174.67	5371383.46	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001373	488164.63	5371371.00	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001374	488154.59	5371358.55	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001375	488144.54	5371346.09	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001376	488134.50	5371333.63	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001377	488124.46	5371321.18	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001378	488114.42	5371308.72	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001379	488104.37	5371296.27	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001380	488094.33	5371283.81	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001381	488084.29	5371271.35	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001382	488074.25	5371258.90	0.00	1.28	0.00004	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001383	487683.50	5371347.67	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001384	487699.49	5371348.09	0.00	1.28	0.00004	16.00		7.44	1.19

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SO1 - 6



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001385	487715.49	5371348.51	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001386	487731.48	5371348.93	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001387	487747.48	5371349.35	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001388	487763.47	5371349.76	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001389	487779.47	5371350.18	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001390	487795.46	5371350.60	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001391	487811.46	5371351.02	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001392	487827.45	5371351.44	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001393	487843.45	5371351.86	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001394	487859.44	5371352.27	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001395	487875.43	5371352.69	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001396	487891.43	5371353.11	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001397	487907.42	5371353.53	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001398	487923.42	5371353.95	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001399	487939.41	5371354.36	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001400	487955.41	5371354.78	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001401	487971.40	5371355.20	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001402	487987.40	5371355.62	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001403	488003.39	5371356.04	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001404	488019.38	5371356.46	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001405	488035.38	5371356.87	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001406	488051.37	5371357.29	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001407	488067.37	5371357.71	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001408	488083.36	5371358.13	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001409	488099.36	5371358.55	0.00	1.28	0.00004	16.00		7.44	1.19

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SO1 - 7



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001410	488115.35	5371358.96	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001411	488131.35	5371359.38	0.00	1.28	0.00004	16.00		7.44	1.19
	L0001412	488147.34	5371359.80	0.00	1.28	0.00004	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001413	487693.32	5371246.10	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001414	487714.31	5371246.67	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001415	487735.30	5371247.24	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001416	487756.29	5371247.80	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001417	487777.29	5371248.37	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001418	487798.28	5371248.94	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001419	487819.27	5371249.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001420	487840.26	5371250.08	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001421	487861.26	5371250.64	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001422	487882.25	5371251.21	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001423	487903.24	5371251.78	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001424	487924.23	5371252.35	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001425	487945.22	5371252.92	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001426	487966.22	5371253.48	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001427	487987.21	5371254.05	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001428	488008.20	5371254.62	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001429	488029.19	5371255.19	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001430	488050.19	5371255.76	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001431	488071.18	5371256.33	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001432	488092.17	5371256.89	0.00	1.28	0.00023	21.00		9.77	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h24.isc AERMOD View by Lakes Environmental Software

SO1 - 8



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE1	L0001433	488113.16	5371257.46	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001434	488134.16	5371258.03	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001435	488155.15	5371258.60	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001436	488176.14	5371259.17	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001437	488197.13	5371259.73	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001438	488218.12	5371260.50	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001439	488239.09	5371261.54	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001440	488260.07	5371262.57	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001441	488281.04	5371263.61	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001442	488301.91	5371265.91	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001443	488322.74	5371268.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001444	488343.18	5371272.96	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001445	488363.21	5371279.26	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001446	488383.25	5371285.56	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001447	488402.64	5371293.59	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001448	488421.94	5371301.86	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001449	488441.05	5371310.51	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001450	488459.13	5371321.20	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001451	488477.21	5371331.88	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001452	488494.81	5371343.28	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001453	488511.76	5371355.68	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001454	488528.71	5371368.08	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001455	488544.43	5371381.86	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001456	488558.66	5371397.30	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001457	488572.90	5371412.74	0.00	1.28	0.00023	21.00		9.77	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h24.isc AERMOD View by Lakes Environmental Software

SO1 - 9



										AERMO
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE1	L0001458	488587.14	5371428.17	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001459	488601.37	5371443.61	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001460	488615.61	5371459.05	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001461	488629.84	5371474.49	0.00	1.28	0.00023	21.00		9.77	1.19
	L0001462	488644.08	5371489.93	0.00	1.28	0.00023	21.00		9.77	1.19

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SO1 - 10



## Source Pathway - Source Inputs - PM2.5 (1hr & Annual)

oint Sources									
Source Type	Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation (Optional)	Release Height [m]	Emission Rate [g/s]	Gas Exit Temp. [K]	Gas Exit Velocity [m/s]	Stack Inside Diameter [m]
POINT	STCK1	488178.53 UNIT Heater	5371354.82	281.00	4.50	0.00006	333.00	0.78	0.10
POINT	1STCK2	488180.66 UNIT Heater	5371353.01	281.00	4.50	0.00006	333.00	0.78	0.10
POINT	STCK3	488186.92 Hot Water Heater	5371347.82	281.00	4.50	0.00014	333.00	2.02	0.10
POINT	STCK4	488194.30 AHU	5371350.44	281.00	2.00	0.00019	333.00	1.20	0.15
POINT	STCK5	488191.80 AHU	5371353.01	281.00	2.00	0.00019	333.00	1.20	0.15
POINT	STCK6	488187.79 Generac SG150	5371360.70	281.00	3.00	0.00013	323.00	18.71	0.20
POINT	NETRAIN	488222.33 Train (Cummins QSK	5371358.38 95) NE bound	281.00	4.40	0.00051	618.75	14.82	0.51
POINT	SWTRAIN	488163.01 Train (Cummins QSK	5371287.60 95) SW bound	281.00	4.40	0.00051	618.85	14.82	0.51

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 1

2025-01-11



Line Volume Sources Source Type: LINE VOLUME Source: SLINE1

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
21.00	0.00019		487682.82	5371245.81	0.00	1.28
			488209.40	5371260.07	0.00	1.28
			488285.16	5371263.82	0.00	1.28
			488333.17	5371269.82	0.00	1.28
			488385.68	5371286.32	0.00	1.28
			488438.19	5371308.82	0.00	1.28
			488487.69	5371338.08	0.00	1.28
			488537.95	5371374.83	0.00	1.28
			488644.47	5371490.35	0.00	1.28

Source Type: LINE VOLUME

Source:	SLINE2	

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00002		488076.72	5371257.50	0.00	1.28
			488072.77	5371821.62	0.00	1.28

#### Source Type: LINE VOLUME Source: SLINE3

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00002		488400.62	5371663.72	0.00	1.28
			488074.16	5371258.79	0.00	1.28

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 2

2025-01-11



Source Type: LINE VOLUME Source: SLINE4

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	0.00002		487675.50	5371347.47	0.00	1.28
			488155.77	5371360.02	0.00	1.28

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 3

2025-01-11



#### Volume Sources Generated from Line Sources

Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE1	L0001561	487693.32	5371246.10	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001562	487714.31	5371246.67	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001563	487735.30	5371247.24	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001564	487756.29	5371247.80	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001565	487777.29	5371248.37	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001566	487798.28	5371248.94	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001567	487819.27	5371249.51	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001568	487840.26	5371250.08	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001569	487861.26	5371250.64	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001570	487882.25	5371251.21	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001571	487903.24	5371251.78	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001572	487924.23	5371252.35	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001573	487945.22	5371252.92	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001574	487966.22	5371253.48	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001575	487987.21	5371254.05	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001576	488008.20	5371254.62	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001577	488029.19	5371255.19	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001578	488050.19	5371255.76	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001579	488071.18	5371256.33	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001580	488092.17	5371256.89	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001581	488113.16	5371257.46	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001582	488134.16	5371258.03	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001583	488155.15	5371258.60	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001584	488176.14	5371259.17	0.00	1.28	3.82E-6	21.00		9.77	1.19

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SO1 - 4

2025-01-11



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001585	488197.13	5371259.73	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001586	488218.12	5371260.50	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001587	488239.09	5371261.54	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001588	488260.07	5371262.57	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001589	488281.04	5371263.61	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001590	488301.91	5371265.91	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001591	488322.74	5371268.51	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001592	488343.18	5371272.96	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001593	488363.21	5371279.26	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001594	488383.25	5371285.56	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001595	488402.64	5371293.59	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001596	488421.94	5371301.86	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001597	488441.05	5371310.51	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001598	488459.13	5371321.20	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001599	488477.21	5371331.88	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001600	488494.81	5371343.28	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001601	488511.76	5371355.68	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001602	488528.71	5371368.08	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001603	488544.43	5371381.86	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001604	488558.66	5371397.30	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001605	488572.90	5371412.74	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001606	488587.14	5371428.17	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001607	488601.37	5371443.61	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001608	488615.61	5371459.05	0.00	1.28	3.82E-6	21.00		9.77	1.19
	L0001609	488629.84	5371474.49	0.00	1.28	3.82E-6	21.00		9.77	1.19

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SO1 - 5



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001610	488644.08	5371489.93	0.00	1.28	3.82E-6	21.00		9.77	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE2	L0001611	488076.67	5371265.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001612	488076.56	5371281.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001613	488076.44	5371297.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001614	488076.33	5371313.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001615	488076.22	5371329.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001616	488076.11	5371345.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001617	488076.00	5371361.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001618	488075.88	5371377.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001619	488075.77	5371393.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001620	488075.66	5371409.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001621	488075.55	5371425.50	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001622	488075.44	5371441.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001623	488075.32	5371457.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001624	488075.21	5371473.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001625	488075.10	5371489.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001626	488074.99	5371505.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001627	488074.88	5371521.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001628	488074.76	5371537.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001629	488074.65	5371553.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001630	488074.54	5371569.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001631	488074.43	5371585.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001632	488074.32	5371601.49	0.00	1.28	6.65E-7	16.00		7.44	1.19

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SO1 - 6



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Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001633	488074.20	5371617.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001634	488074.09	5371633.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001635	488073.98	5371649.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001636	488073.87	5371665.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001637	488073.76	5371681.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001638	488073.64	5371697.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001639	488073.53	5371713.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001640	488073.42	5371729.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001641	488073.31	5371745.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001642	488073.20	5371761.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001643	488073.08	5371777.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001644	488072.97	5371793.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
	L0001645	488072.86	5371809.49	0.00	1.28	6.65E-7	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001646	488395.60	5371657.49	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001647	488385.56	5371645.04	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001648	488375.51	5371632.58	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001649	488365.47	5371620.13	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001650	488355.43	5371607.67	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001651	488345.39	5371595.21	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001652	488335.34	5371582.76	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001653	488325.30	5371570.30	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001654	488315.26	5371557.85	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001655	488305.22	5371545.39	0.00	1.28	7.05E-7	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 7



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001656	488295.18	5371532.93	0.00	1.28	7.05E-7	16.00		Initial Lateral Dimencion [m] 7.44 7.44 7.44 7.44 7.44 7.44 7.44 7.4	1.19
	L0001657	488285.13	5371520.48	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001658	488275.09	5371508.02	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001659	488265.05	5371495.56	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001660	488255.01	5371483.11	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001661	488244.97	5371470.65	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001662	488234.92	5371458.20	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001663	488224.88	5371445.74	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001664	488214.84	5371433.28	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001665	488204.80	5371420.83	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001666	488194.75	5371408.37	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001667	488184.71	5371395.92	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001668	488174.67	5371383.46	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001669	488164.63	5371371.00	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001670	488154.59	5371358.55	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001671	488144.54	5371346.09	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001672	488134.50	5371333.63	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001673	488124.46	5371321.18	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001674	488114.42	5371308.72	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001675	488104.37	5371296.27	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001676	488094.33	5371283.81	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001677	488084.29	5371271.35	0.00	1.28	7.05E-7	16.00		7.44	1.19
	L0001678	488074.25	5371258.90	0.00	1.28	7.05E-7	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 8



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001679	487683.50	5371347.67	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001680	487699.49	5371348.09	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001681	487715.49	5371348.51	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001682	487731.48	5371348.93	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001683	487747.48	5371349.35	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001684	487763.47	5371349.76	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001685	487779.47	5371350.18	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001686	487795.46	5371350.60	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001687	487811.46	5371351.02	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001688	487827.45	5371351.44	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001689	487843.45	5371351.86	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001690	487859.44	5371352.27	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001691	487875.43	5371352.69	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001692	487891.43	5371353.11	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001693	487907.42	5371353.53	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001694	487923.42	5371353.95	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001695	487939.41	5371354.36	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001696	487955.41	5371354.78	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001697	487971.40	5371355.20	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001698	487987.40	5371355.62	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001699	488003.39	5371356.04	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001700	488019.38	5371356.46	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001701	488035.38	5371356.87	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001702	488051.37	5371357.29	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001703	488067.37	5371357.71	0.00	1.28	7.75E-7	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

SO1 - 9



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Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE4	L0001704	488083.36	5371358.13	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001705	488099.36	5371358.55	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001706	488115.35	5371358.96	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001707	488131.35	5371359.38	0.00	1.28	7.75E-7	16.00		7.44	1.19
	L0001708	488147.34	5371359.80	0.00	1.28	7.75E-7	16.00		7.44	1.19

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SO1 - 10



## Source Pathway - Source Inputs Benzene (24hr & Annual)

Point Sources									
Source Type	Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation (Optional)	Release Height [m]	Emission Rate [g/s]	Gas Exit Temp. [K]	Gas Exit Velocity [m/s]	Stack Inside Diameter [m]
POINT	STCK1	488178.53 UNIT Heater	5371354.82	281.00	4.50	1.50E-11	333.00	0.78	0.10
POINT	1STCK2	488180.66 UNIT Heater	5371353.01	281.00	4.50	1.50E-11	333.00	0.78	0.10
POINT	STCK3	488186.92 Hot Water Heater	5371347.82	281.00	4.50	3.70E-11	333.00	2.02	0.10
POINT	STCK4	488194.30 AHU	5371350.44	281.00	2.00	4.90E-11	333.00	1.20	0.15
POINT	STCK5	488191.80 AHU	5371353.01	281.00	2.00	4.90E-11	333.00	1.20	0.15
POINT	STCK6	488187.79 Generac SG150	5371360.70	281.00	3.00	0.00002	323.00	18.71	0.20
POINT	NETRAIN	488222.33 Train (Cummins QSK	5371358.38 95) NE bound	281.00	4.40	0.00005	618.75	14.82	0.51
POINT	SWTRAIN	488163.01 Train (Cummins QSK	5371287.60 95) SW bound	281.00	4.40	0.00005	618.85	14.82	0.51

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 1

2025-01-11



Line Volume Sources Source Type: LINE VOLUME Source: SLINE1

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
21.00	0.00002		487682.82	5371245.81	0.00	1.28
			488209.40	5371260.07	0.00	1.28
			488285.16	5371263.82	0.00	1.28
			488333.17	5371269.82	0.00	1.28
			488385.68	5371286.32	0.00	1.28
			488438.19	5371308.82	0.00	1.28
			488487.69	5371338.08	0.00	1.28
			488537.95	5371374.83	0.00	1.28
			488644.47	5371490.35	0.00	1.28

Source Type: LINE VOLUME

Source:	SLINE2	

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	1.98E-6		488076.72	5371257.50	0.00	1.28
			488072.77	5371821.62	0.00	1.28

#### Source Type: LINE VOLUME Source: SLINE3

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	1.98E-6		488400.62	5371663.72	0.00	1.28
			488074.16	5371258.79	0.00	1.28

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 2



Source Type: LINE VOLUME Source: SLINE4

Length of Side [m]	Emission Rate [g/ s]	Building Height [m]	X Coordinate for Points [m]	Y Coordinate for points [m]	Base Elevation [m]	Release Height [m]
16.00	1.98E-6		487675.50	5371347.47	0.00	1.28
			488155.77	5371360.02	0.00	1.28

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 3

2025-01-11



#### Volume Sources Generated from Line Sources

Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE1	L0001709	487693.32	5371246.10	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001710	487714.31	5371246.67	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001711	487735.30	5371247.24	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001712	487756.29	5371247.80	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001713	487777.29	5371248.37	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001714	487798.28	5371248.94	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001715	487819.27	5371249.51	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001716	487840.26	5371250.08	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001717	487861.26	5371250.64	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001718	487882.25	5371251.21	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001719	487903.24	5371251.78	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001720	487924.23	5371252.35	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001721	487945.22	5371252.92	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001722	487966.22	5371253.48	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001723	487987.21	5371254.05	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001724	488008.20	5371254.62	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001725	488029.19	5371255.19	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001726	488050.19	5371255.76	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001727	488071.18	5371256.33	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001728	488092.17	5371256.89	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001729	488113.16	5371257.46	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001730	488134.16	5371258.03	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001731	488155.15	5371258.60	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001732	488176.14	5371259.17	0.00	1.28	3.75E-7	21.00		9.77	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 4

2025-01-11



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001733	488197.13	5371259.73	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001734	488218.12	5371260.50	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001735	488239.09	5371261.54	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001736	488260.07	5371262.57	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001737	488281.04	5371263.61	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001738	488301.91	5371265.91	0.00	1.28	3.75E-7	21.00		9.77	1.19
L0001739	488322.74	5371268.51	0.00	1.28	3.75E-7	21.00		9.77	1.19	
	L0001740	488343.18	5371272.96	0.00	1.28	3.75E-7	21.00		9.77	1.19
L0001741 L0001742 L0001743	488363.21	5371279.26	0.00	1.28	3.75E-7	21.00		9.77	1.19	
	L0001742	488383.25	5371285.56	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001743	488402.64	5371293.59	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001744	488421.94	5371301.86	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001745	488441.05	5371310.51	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001746	488459.13	5371321.20	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001747	488477.21	5371331.88	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001748	488494.81	5371343.28	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001749	488511.76	5371355.68	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001750	488528.71	5371368.08	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001751	488544.43	5371381.86	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001752	488558.66	5371397.30	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001753	488572.90	5371412.74	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001754	488587.14	5371428.17	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001755	488601.37	5371443.61	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001756	488615.61	5371459.05	0.00	1.28	3.75E-7	21.00		9.77	1.19
	L0001757	488629.84	5371474.49	0.00	1.28	3.75E-7	21.00		9.77	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 5



	·									AERM
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE1	L0001758	488644.08	5371489.93	0.00	1.28	3.75E-7	21.00		9.77	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE2	L0001759	488076.67	5371265.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001760	488076.56	5371281.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001761	488076.44	5371297.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001762	488076.33	5371313.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001763	488076.22	5371329.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
L00017 L00017	L0001764	488076.11	5371345.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001765	488076.00	5371361.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001766	488075.88	5371377.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001767	488075.77	5371393.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001768	488075.66	5371409.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001769	488075.55	5371425.50	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001770	488075.44	5371441.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001771	488075.32	5371457.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001772	488075.21	5371473.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001773	488075.10	5371489.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001774	488074.99	5371505.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001775	488074.88	5371521.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001776	488074.76	5371537.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001777	488074.65	5371553.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001778	488074.54	5371569.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001779	488074.43	5371585.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001780	488074.32	5371601.49	0.00	1.28	5.65E-8	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 6



										AERM
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE2	L0001781	488074.20	5371617.49	0.00	1.28	5.65E-8	16.00		Initial Lateral Dimencion [m]   7.44	1.19
	L0001782	488074.09	5371633.49	0.00	1.28	5.65E-8	16.00			1.19
	L0001783	488073.98	5371649.49	0.00	1.28	5.65E-8	16.00			1.19
	L0001784	488073.87	5371665.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001785	488073.76	5371681.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001786	488073.64	5371697.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001787	488073.53	5371713.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001788	488073.42	5371729.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001789	488073.31	5371745.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001790	488073.20	5371761.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
L00017	L0001791	488073.08	5371777.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001792	488072.97	5371793.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
	L0001793	488072.86	5371809.49	0.00	1.28	5.65E-8	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001794	488395.60	5371657.49	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001795	488385.56	5371645.04	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001796	488375.51	5371632.58	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001797	488365.47	5371620.13	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001798	488355.43	5371607.67	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001799	488345.39	5371595.21	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001800	488335.34	5371582.76	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001801	488325.30	5371570.30	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001802	488315.26	5371557.85	0.00	1.28	5.99E-8	16.00		7.44	1.19
	1.0001.002	100005.00	5071515.00	2022	100000	100000000000000	105200100000		7.44	1000000

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 7



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE3	L0001804	488295.18	5371532.93	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001805	488285.13	5371520.48	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001806	488275.09	5371508.02	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001807	488265.05	5371495.56	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001808	488255.01	5371483.11	0.00	1.28	5.99E-8	16.00		7.44	1.19
L000180 L000181 L000181 L000181 L000181	L0001809	488244.97	5371470.65	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001810	488234.92	5371458.20	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001811	488224.88	5371445.74	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001812	488214.84	5371433.28	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001813	488204.80	5371420.83	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001814	488194.75	5371408.37	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001815	488184.71	5371395.92	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001816	488174.67	5371383.46	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001817	488164.63	5371371.00	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001818	488154.59	5371358.55	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001819	488144.54	5371346.09	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001820	488134.50	5371333.63	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001821	488124.46	5371321.18	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001822	488114.42	5371308.72	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001823	488104.37	5371296.27	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001824	488094.33	5371283.81	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001825	488084.29	5371271.35	0.00	1.28	5.99E-8	16.00		7.44	1.19
	L0001826	488074.25	5371258.90	0.00	1.28	5.99E-8	16.00		7.44	1.19
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 8



Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertica Dimencion [m]
SLINE4	L0001827	487683.50	5371347.67	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001828	487699.49	5371348.09	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001829	487715.49	5371348.51	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001830	487731.48	5371348.93	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001831	487747.48	5371349.35	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001832	487763.47	5371349.76	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001833	487779.47	5371350.18	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001834	487795.46	5371350.60	0.00	1.28	6.59E-8	16.00		7.44	1.19
L0001835	487811.46	5371351.02	0.00	1.28	6.59E-8	16.00		7.44	1.19	
	L0001836	487827.45	5371351.44	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001837	487843.45	5371351.86	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001838	487859.44	5371352.27	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001839	487875.43	5371352.69	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001840	487891.43	5371353.11	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001841	487907.42	5371353.53	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001842	487923.42	5371353.95	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001843	487939.41	5371354.36	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001844	487955.41	5371354.78	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001845	487971.40	5371355.20	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001846	487987.40	5371355.62	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001847	488003.39	5371356.04	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001848	488019.38	5371356.46	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001849	488035.38	5371356.87	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001850	488051.37	5371357.29	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001851	488067.37	5371357.71	0.00	1.28	6.59E-8	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 9



	×	540 -								AERMO
Line Source ID	Volume Source ID	X Coordinate [m]	Y Coordinate [m]	Base Elevation [m]	Release Height [m[	Emission Rate [g/s]	Length of Side [m]	Building Height [m]	Initial Lateral Dimencion [m]	Initial Vertical Dimencion [m]
SLINE4	L0001852	488083.36	5371358.13	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001853	488099.36	5371358.55	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001854	488115.35	5371358.96	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001855	488131.35	5371359.38	0.00	1.28	6.59E-8	16.00		7.44	1.19
	L0001856	488147.34	5371359.80	0.00	1.28	6.59E-8	16.00		7.44	1.19

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

SO1 - 10



# Source Pathway - NO2, PM2.5, Benzene

#### **Building Downwash Information**

Source ID: STCK1 Heights [m] (10 to 360 deg) 10-60 deg 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 70-120 deg 130-180 deg 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 7.50 190-240 deg 250-300 deg 7.50 7.50 7.50 7.50 7.50 7.50 310-360 deg 7.50 7.50 7.50 7.50 7.50 7.50 Widths [m] (10 to 360 deg) 10-60 deg 39.43 35.49 30.48 27.54 30.43 35.48 70-120 deg 39.46 42.24 43.73 43.90 42.73 41.08 130-180 dea 40.14 41.17 42.57 43.76 43.63 42.17 190-240 deg 39 43 35 49 30 48 27 54 30 43 35 48 250-300 deg 39.46 42.24 43.73 43.90 42.73 41.08 310-360 deg 40.14 41.17 42.57 43.76 43.63 42.17 Lengths [m] (10 to 360 deg) 10-60 deg 43.90 42.73 41.08 40.14 41.17 42.57 43.76 43.63 42.17 39.43 35.49 30.48 70-120 deg 130-180 deg 27.54 30.43 35.48 39.46 42.24 43.73 190-240 deg 43.90 42 73 41 08 40 14 41.17 42 57 250-300 deg 43.76 43.63 42.17 39.43 35.49 30,48 310-360 deg 27.54 30.43 35.48 39.46 42.24 43.73 Along Flow [m] (10 to 360 deg) 10-60 deg -42.90 -41.87 -40.38 -38.08 -36.49 -34.18 70-120 deg -31.71 -28.28 -23.99 -18.97 -13.37 -7.37 130-180 dea -2.67 -1.20 -1.23 -1.23 -1.19 -1.11 -8.38 190-240 deg -1.00 -0.86 -0.69 -2.07 -4.68 -12.05 -15.35 -18.18 -20.46 -22.12 -23.10 250-300 deg 310-360 deg -24.87 -29.23 -34.25 -38.23 -41.05 -42.62 Across Flow [m] (10 to 360 deg) 10-60 deg -0.74 -4.37 -7.87 -11.10 -14.02 -16.51 -18.50 -19.93 -20.75 -20.95 -20.51 -19.85 70-120 deg 130-180 deg -18.01 -15.90 -12.90 -9.83 -6.47 -2.90 074 4 37 7 87 11 10 14 02 16 51 190-240 deg 18.50 19.93 20.76 20.95 20.51 19.85 250-300 deg 310-360 deg 18.01 15.90 12.90 9.83 6.47 2.90 1STCK2 Source ID: Heights [m] (10 to 360 deg)

10-60 deg 7.50 7.50 7.50 7.50 7.50

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 1

2025-01-11

7.50



						AERMOD
70-120 deg	7.50	7.50	7.50	7.50	7.50	7.50
130-180 deg	7.50	7.50	7.50	7.50	7.50	7.50
190-240 deg	7.50	7.50	7.50	7.50	7.50	7.50
250-300 deg	7.50	7.50	7.50	7.50	7.50	7.50
310-360 deg	7.50	7.50	7.50	7.50	7.50	7.50
Widths [m] (10 to 360 c	leg)					
10-60 deg	39.43	35.49	30.48	27.54	30.43	35.48
70-120 deg	39.46	42.24	43.73	43.90	42.73	41.08
130-180 deg	40.14	41.17	42.57	43.76	43.63	42.17
190-240 deg	39.43	35.49	30.48	27.54	30.43	35.48
250-300 deg	39.46	42.24	43.73	43.90	42.73	41.08
310-360 deg	40.14	41.17	42.57	43.76	43.63	42.17
Lengths [m] (10 to 360	deg)					
10-60 deg	43.90	42.73	41.08	40.14	41.17	42.57
70-120 deg	43.76	43.63	42.17	39.43	35.49	30.48
130-180 deg	27.54	30.43	35.48	39.46	42.24	43.73
190-240 deg	43.90	42.73	41.08	40.14	41.17	42.57
250-300 deg	43.76	43.63	42.17	39.43	35.49	30.48
310-360 deg	27.54	30.43	35.48	39.46	42.24	43.73
Along Flow [m] (10 to 3	360 deg)					
10-60 deg	-41.48	-40.90	-39.88	-38.06	-36.96	-35.12
70-120 deg	-33.10	-30.06	-26.12	-21.38	-15.99	-10.12
130-180 deg	-5.47	-3.95	-3.86	-3.66	-3.34	-2.92
190-240 deg	-2.41	-1.83	-1.19	-2.08	-4.21	-7.44
250-300 deg	-10.67	-13.56	-16.05	-18.05	-19.50	-20.35
310-360 deg	-22.07	-26.47	-31.62	-35.80	-38.90	-40.81
Across Flow [m] (10 to	360 deg)					
10-60 deg	1.67	-1.75	-5.12	-8.30	-11.26	-13.88
70-120 deg	-16.07	-17.78	-18.95	-19.54	-19.53	-19.34
130-180 deg	-17.99	-16.37	-13.84	-11.21	-8.25	-5.03
190-240 deg	-1.67	1.75	5.12	8.30	11.26	13.88
250-300 deg	16.07	17.78	18.95	19.54	19.53	19.34
310-360 deg	17.99	16.37	13.84	11.21	8.25	5.03
Source ID: STO	СКЗ					
Heights [m] (10 to 360	deg)					
10-60 deg	7.50	7.50	7.50	7.50	7.50	7.50
70-120 deg	7.50	7.50	7.50	7.50	7.50	7.50
130-180 deg	7.50	7.50	7.50	7.50	7.50	7.50
190-240 deg	7.50	7.50	7.50	7.50	7.50	7.50
250-300 deg	7.50	7.50	7.50	7.50	7.50	7.50
310-360 deg	7.50	7.50	7.50	7.50	7.50	7.50

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 2



Widths [m] (10 to 360 d	leg)					
10-60 deg	39.43	35.49	30.48	27.54	30.43	35.48
70-120 deg	39.46	42.24	43.73	43.90	42.73	41.08
130-180 deg	40.14	41.17	42.57	43.76	43.63	42.17
190-240 deg	39.43	35.49	30.48	27.54	30.43	35.48
250-300 deg	39.46	42.24	43.73	43.90	42.73	41.08
310-360 deg	40.14	41.17	42.57	43.76	43.63	42.17
Lengths [m] (10 to 360	deg)					
10-60 deg	43.90	42.73	41.08	40.14	41.17	42.57
70-120 deg	43.76	43.63	42.17	39.43	35.49	30.48
130-180 deg	27.54	30.43	35.48	39.46	42.24	43.73
190-240 deg	43.90	42.73	41.08	40.14	41.17	42.57
250-300 deg	43.76	43.63	42.17	39.43	35.49	30.48
310-360 deg	27.54	30.43	35.48	39.46	42.24	43.73
Along Flow [m] (10 to 3	360 deg)					
10-60 deg	-37.46	-38.16	-38.52	-38.11	-38.42	-37.95
70-120 deg	-37.20	-35.33	-32.38	-28.45	-23.65	-18.14
130-180 deg	-13.60	-11.95	-11.49	-10.68	-9.54	-8.11
190-240 deg	-6.44	-4.57	-2.56	-2.03	-2.75	-4.62
250-300 deg	-6.56	-8.30	-9.79	-10.98	-11.84	-12.34
310-360 deg	-13.94	-18.47	-23.99	-28.78	-32.70	-35.62
Across Flow [m] (10 to	360 deg)					
10-60 deg	8.73	5.91	2.90	-0.17	-3.26	-6.25
70-120 deg	-9.05	-11.58	-13.76	-15.51	-16.80	-17.98
130-180 deg	-18.04	-17.83	-16.66	-15.32	-13.51	-11.29
190-240 deg	-8.73	-5.91	-2.90	0.17	3.26	6.25
250-300 deg	9.05	11.58	13.76	15.51	16.80	17.98
310-360 deg	18.04	17.83	16.66	15.32	13.51	11.29
Source ID: STO						
Heights [m] (10 to 360	aeg)					
10-60 deg	7.50	7.50	7.50	7.50	7.50	7.50

Heights [m] (10 to 360 d	ieg)					
10-60 deg	7.50	7.50	7.50	7.50	7.50	7.50
70-120 deg	7.50	7.50	7.50	7.50	7.50	7.50
130-180 deg	0.00	0.00	7.50	7.50	7.50	7.50
190-240 deg	7.50	7.50	7.50	7.50	7.50	7.50
250-300 deg	7.50	7.50	7.50	7.50	7.50	7.50
310-360 deg	4.39	4.39	7.50	7.50	7.50	7.50
Widths [m] (10 to 360 d	eg)					
10-60 deg	39.43	35.49	30.48	27.54	30.43	35.48
70-120 deg	39.46	42.24	43.73	43.90	42.73	41.08
130-180 deg	0.00	0.00	42.57	43.76	43.63	42.17
190-240 deg	39.43	35.49	30.48	27.54	30.43	35.48

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc SO2 - 3

AERMOD View by Lakes Environmental Software

2025-01-11



	ile.					AERMOD
250-300 deg	39.46	42.24	43.73	43.90	42.73	41.08
310-360 deg	103.40	102.35	42.57	43.76	43.63	42.17
Lengths [m] (10 to 360	deg)					
10-60 deg	43.90	42.73	41.08	40.14	41.17	42.57
70-120 deg	43.76	43.63	42.17	39.43	35.49	30.48
130-180 deg	0.00	0.00	35.48	39.46	42.24	43.73
190-240 deg	43.90	42.73	41.08	40.14	41.17	42.57
250-300 deg	43.76	43.63	42.17	39.43	35.49	30.48
310-360 deg	3.01	20.92	35.48	39.46	42.24	43.73
Along Flow [m] (10 to	360 deg)					
10-60 deg	-41.32	-43.15	-44.48	-44.86	-45.76	-45.65
70-120 deg	-45.03	-43.05	-39.76	-35.26	-29.69	-23.22
130-180 deg	0.00	0.00	-12.91	-10.74	-8.24	-5.49
190-240 deg	-2.57	0.42	3.40	4.72	4.58	3.08
250-300 deg	1.27	-0.58	-2.41	-4.17	-5.80	-7.26
310-360 deg	-17.96	-30.50	-22.57	-28.72	-34.00	-38.24
Across Flow [m] (10 to	o 360 deg)					
10-60 deg	15.55	11.94	7.98	3.80	-0.52	-4.83
70-120 deg	-8.99	-12.88	-16.38	-19.37	-21.78	-23.94
130-180 deg	0.00	0.00	-24.37	-23.15	-21.24	-18.67
190-240 deg	-15.55	-11.94	-7.98	-3.80	0.52	4.83
250-300 deg	8.99	12.88	16.38	19.37	21.78	23.94
310-360 deg	22.10	18.91	24.37	23.15	21.24	18.67

Source ID: ST	CK5					
Heights [m] (10 to 360	deg)					
10-60 deg	7.50	7.50	7.50	7.50	7.50	7.50
70-120 deg	7.50	7.50	7.50	7.50	7.50	4.39
130-180 deg	0.00	0.00	7.50	7.50	7.50	7.50
190-240 deg	7.50	7.50	7.50	7.50	7.50	7.50
250-300 deg	7.50	7.50	7.50	7.50	7.50	4.39
310-360 deg	4.39	4.39	7.50	7.50	7.50	7.50
Widths [m] (10 to 360	deg)					
10-60 deg	39.43	35.49	30.48	27.54	30.43	35.48
70-120 deg	39.46	42.24	43.73	43.90	42.73	102.35
130-180 deg	0.00	0.00	42.57	43.76	43.63	42.17
190-240 deg	39.43	35.49	30.48	27.54	30.43	35.48
250-300 deg	39.46	42.24	43.73	43.90	42.73	102.35
310-360 deg	103.40	102.35	42.57	43.76	43.63	42.17
Lengths [m] (10 to 360	deg)					
10-60 deg	43.90	42.73	41.08	40.14	41.17	42.57
70-120 deg	43.76	43.63	42.17	39.43	35.49	20.91

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 4



						AERMOD
130-180 deg	0.00	0.00	35.48	39.46	42.24	43.73
190-240 deg	43.90	42.73	41.08	40.14	41.17	42.57
250-300 deg	43.76	43.63	42.17	39.43	35.49	20.91
310-360 deg	3.01	20.92	35.48	39.46	42.24	43.73
Along Flow [m] (10 to	360 deg)					
10-60 deg	-43.42	-44.71	-45.45	-45.22	-45.49	-44.77
70-120 deg	-43.56	-41.04	-37.26	-32.35	-26.46	5.37
130-180 deg	0.00	0.00	-9.43	-7.47	-5.27	-2.92
190-240 deg	-0.48	1.98	4.38	5.08	4.32	2.20
250-300 deg	-0.20	-2.59	-4.91	-7.08	-9.03	-26.27
310-360 deg	-21.53	-34.08	-26.05	-31.99	-36.96	-40.81
Across Flow [m] (10 to	o 360 deg)					
10-60 deg	12.64	8.72	4.53	0.23	-4.10	-8.31
70-120 deg	-12.26	-15.84	-18.95	-21.47	-23.34	-25.60
130-180 deg	0.00	0.00	-23.49	-21.68	-19.22	-16.17
190-240 deg	-12.64	-8.72	-4.53	-0.23	4.10	8.31
250-300 deg	12.26	15.84	18.95	21.47	23.34	25.60
310-360 deg	22.46	18.65	23.49	21.68	19.22	16.17

Source ID: ST	-K6					
Heights [m] (10 to 360	deg)					
10-60 deg	7.50	7.50	7.50	7.50	7.50	7.50
70-120 deg	7.50	7.50	0.00	0.00	0.00	0.00
130-180 deg	0.00	0.00	7.50	7.50	7.50	7.50
190-240 deg	7.50	7.50	7.50	7.50	7.50	7.50
250-300 deg	7.50	7.50	0.00	0.00	0.00	0.00
310-360 deg	0.00	0.00	7.50	7.50	7.50	7.50
Widths [m] (10 to 360 c	leg)					
10-60 deg	39.43	35.49	30.48	27.54	30.43	35.48
70-120 deg	39.46	42.24	0.00	0.00	0.00	0.00
130-180 deg	0.00	0.00	42.57	43.76	43.63	42.17
190-240 deg	39.43	35.49	30.48	27.54	30.43	35.48
250-300 deg	39.46	42.24	0.00	0.00	0.00	0.00
310-360 deg	0.00	0.00	42.57	43.76	43.63	42.17
Lengths [m] (10 to 360	deg)					
10-60 deg	43.90	42.73	41.08	40.14	41.17	42.57
70-120 deg	43.76	43.63	0.00	0.00	0.00	0.00
130-180 deg	0.00	0.00	35.48	39.46	42.24	43.73
190-240 deg	43.90	42.73	41.08	40.14	41.17	42.57
250-300 deg	43.76	43.63	0.00	0.00	0.00	0.00
310-360 deg	0.00	0.00	35.48	39.46	42.24	43.73

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 5



Along Flow [m] (10 to 3	360 deg)					
10-60 deg	-50.29	-50.56	-50.11	-48.53	-47.36	-45.14
70-120 deg	-42.43	-38.42	0.00	0.00	0.00	0.00
130-180 deg	0.00	0.00	-0.77	1.13	3.00	4.77
190-240 deg	6.40	7.83	9.03	8.39	6.19	2.58
250-300 deg	-1.34	-5.21	0.00	0.00	0.00	0.00
310-360 deg	0.00	0.00	-34.71	-40.59	-45.23	-48.50
Across Flow [m] (10 to	) 360 deg)					
10-60 deg	7.35	2.32	-2.79	-7.78	-12.57	-16.97
70-120 deg	-20.86	-24.11	0.00	0.00	0.00	0.00
130-180 deg	0.00	0.00	-23.86	-20.54	-16.61	-12.16
190-240 deg	-7.35	-2.32	2.79	7.78	12.57	16.97
250-300 deg	20.86	24.11	0.00	0.00	0.00	0.00
310-360 deg	0.00	0.00	23.86	20.54	16.61	12.16
Source ID: NE	TRAIN					
Heights [m] (10 to 360	deg)					
10-60 deg	4.39	4.39	4.39	4.39	7.50	7.50
70-120 deg	7.50	7.50	7.50	4.39	4.39	4.39
130-180 deg	4.39	4.39	4.39	4.39	4.39	4.39
190-240 deg	4.39	4.39	4.39	4.39	4.39	4.39
250-300 deg	4.39	4.39	4.39	4.39	4.39	4.39
310-360 deg	4.39	4.39	4.39	4.39	4.39	4.39
Widths [m] (10 to 360 o	deg)					
10-60 deg	54.30	38.18	20.91	3.01	30.43	35.48
70-120 deg	39.46	42.24	43.73	91.05	98.19	102.35
130-180 deg	103.40	102.35	98.19	91.04	81.13	68.76
190-240 deg	54.30	38.18	20.91	3.01	20.92	38.19
250-300 deg	54.30	68.77	81.14	91.05	98.19	102.35
310-360 deg	103.40	102.35	98.19	91.04	81.13	68.76
Lengths [m] (10 to 360	deg)					
10-60 deg	91.05	98.19	102.35	103.40	41.17	42.57
70-120 deg	43.76	43.63	42.17	54.30	38.18	20.91
130-180 deg	3.01	20.92	38.19	54.30	68.77	81.14
190-240 deg	91.05	98.19	102.35	103.40	102.35	98.19
250-300 deg	91.04	81.13	68.76	54.30	38.18	20.91
310-360 deg	3.01	20.92	38.19	54.30	68.77	81.14
Along Flow [m] (10 to	360 deg)					
10-60 deg	-85.58	-92.54	-96.69	-97.90	-72.33	-73.89
70-120 deg	-74.09	-72.03	-67.79	-50.17	-34.81	-18.39
130-180 deg	-1.41	-2.35	-3.21	-3.97	-4.62	-5.12

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc SO2 - 6

-5.65

-5.66

-5.50

-5.69

AERMOD View by Lakes Environmental Software

-5.47

2025-01-11

-5.71

AERMOD



190-240 deg
						AERMOD
250-300 deg	-5.55	-5.23	-4.75	-4.12	-3.37	-2.52
310-360 deg	-1.59	-18.57	-34.98	-50.33	-64.15	-76.02
Across Flow [m] (10 to	360 deg)					
10-60 deg	23.02	15.72	7.94	-0.09	11.41	2.31
70-120 deg	-6.87	-15.83	-24.32	-40.06	-43.45	-45.52
130-180 deg	-46.20	-45.48	-43.39	-39.97	-35.34	-29.63
190-240 deg	-23.02	-15.72	-7.94	0.09	8.11	15.89
250-300 deg	23.18	29.77	35.45	40.06	43.45	45.52
310-360 deg	46.20	45.48	43.39	39.97	35.34	29.63
Source ID: SW	TRAIN					
Heights [m] (10 to 360 (	deg)					
10-60 deg	4.39	4.39	4.39	4.39	4.39	4.39
70-120 deg	4.39	4.39	4.39	4.39	4.39	4.39
130-180 deg	4.39	4.39	4.39	4.39	7.50	7.50
190-240 deg	7.50	7.50	7.50	4.39	4.39	4.39
250-300 deg	4.39	4.39	4.39	4.39	4.39	4.39
310-360 deg	4.39	4.39	4.39	4.39	4.39	4.39
Widths [m] (10 to 360 d	eg)					
10-60 deg	54.30	38.18	20.91	3.01	20.92	38.19
70-120 deg	54.30	68.77	81.14	91.05	98.19	102.35
130-180 deg	103.40	102.35	98.19	91.04	43.63	42.17
190-240 deg	39.43	35.49	30.48	3.01	20.92	38.19
250-300 deg	54.30	68.77	81.14	91.05	98.19	102.35
310-360 deg	103.40	102.35	98.19	91.04	81.13	68.76
Lengths [m] (10 to 360	deg)					
10-60 deg	91.05	98.19	102.35	103.40	102.35	98.19
70-120 deg	91.04	81.13	68.76	54.30	38.18	20.91
130-180 deg	3.01	20.92	38.19	54.30	42.24	43.73
190-240 deg	43.90	42.73	41.08	103.40	102.35	98.19
250-300 deg	91.04	81.13	68.76	54.30	38.18	20.91
310-360 deg	3.01	20.92	38.19	54.30	68.77	81.14
Along Flow [m] (10 to 3	60 deg)					
10-60 deg	-5.58	-5.74	-5.73	-5.55	-5.72	-5.72
70-120 deg	-5.54	-5.19	-4.69	-4.04	-3.28	-2.41
130-180 deg	-1.47	-18.44	-34.85	-50.20	-64.69	-68.33
190-240 deg	-69.89	-69.33	-66.67	-97.85	-96.63	-92.47
250-300 deg	-85.51	-75.94	-64.07	-50.25	-34.91	-18.50
310-360 deg	-1.54	-2.48	-3.34	-4.11	-4.75	-5.24
Across Flow [m] (10 to	360 deg)					
10-60 deg	-23.10	-15.82	-8.05	-0.03	7.98	15.75
70-120 deg	23.04	29.64	35.33	39.95	43.35	45.44

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 7



						AERMOD
130-180 deg	46.15	45.45	43.38	39.98	20.49	12.61
190-240 deg	4.36	-4.03	-12.30	0.03	-7.98	-15.75
250-300 deg	-23.04	-29.64	-35.33	-39.95	-43.35	-45.44
310-360 deg	-46.15	-45.45	-43.38	-39.98	-35.37	-29.69

#### **Emission Rate Units for Output**

For Concentration	
Unit Factor:	1E6
Emission Unit Label:	GRAMS/SEC
Concentration Unit Label:	MICROGRAMS/M**3

#### Source Groups

Source Group ID: SWtrain	List of Sources in Group (Source Range or Single Sources)
	STCK1
	1STCK2
	STCK3
	STCK4
	STCK5
	STCK6
	SWTRAIN
Source Group ID: Roads	List of Sources in Group (Source Range or Single Sources)
	SLINE1
	SLINE2
	SLINE3
	SLINE4
Source Group ID: NEtrain	List of Sources in Group (Source Range or Single Sources)
	STCK1
	1STCK2
	STCK3
	STCK4
	STCK5
	STCK6
	NETRAIN

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software SO2 - 8



Data for Particulate	S		0.00	True	True
Source ID: 1STCK2					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]	 	 		
Source ID: NETRAIN					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]	 			
Source ID: SLINE1					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]	 			
Source ID: SLINE2					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]				
Source ID: SLINE3					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]	 			
Source ID: SLINE4					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]	 	 		
Source ID: STCK1					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]				
Source ID: STCK3					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]				
Source ID: STCK4					
Fine Particle Fraction:	1.00				
Mass Mean Particle Diameter:	2.50 [microns]		 		
Source ID: STCK5					
Fine Particle Fraction:	1.00	 			
Mass Mean Particle Diameter:	2.50 [microns]	 	 		

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software SO2 - 9

2025-01-11

AERMOD



Fine Particle Fraction:	1.00	
Mass Mean Particle Diameter:	2.50 [microns]	

#### Source ID: SWTRAIN

 Fine Particle Fraction:
 1.00

 Mass Mean Particle Diameter:
 2.50 [microns]

#### 0.00

AERMOD

## Data for Gases

Source Groups

Source Group ID: SWtrain	List of Sources in Group (Source Range or Single Sources)
	STCK1
	1STCK2
	STCK3
	STCK4
	STCK5
	STCK6
	SWTRAIN
Source Group ID: Roads	List of Sources in Group (Source Range or Single Sources)
	SLINE1
	SLINE2
	SLINE3
	SLINE4
Source Group ID: NEtrain	List of Sources in Group (Source Range or Single Sources)
	STCK1
	1STCK2
	STCK3
	STCK4
	STCK5
	STCK6
	NETRAIN

Project File: D:\Projects\2024\24120 Timmins\JANUARY & 2025\PM25h1.isc AERMOD View by Lakes Environmental Software SO2 - 10



# Meteorology - NO2, PM2.5, Benzene

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Met Input	Data			
Surface Met	Data			
Filename:	Data\Met\Sudbury_forest_22112.SFC			
Format Type:	Default AERMET format			
Profile Met I	Data			
Filename:	Data\Met\Sudbury_forest_22112.PFL			
Format Type:	Default AERMET format			
Wind Speed				Wind Direction
Wind S	peeds are Vector Mean (Not Scalar Means)			Rotation Adjustment [deg]:
Potential Te	mperature Profile			•
Base Elevatio	n above MSL (for Primary Met Tower):	348.00	[m]	

#### **Meteorological Station Data**

Stations	Station No.	Year	X Coordinate [m]	Y Coordinate [m]	Station Name
Surface		1996			SUDBURY
Upper Air		1996			WHITE LAKE

#### Data Period

Data Period to Process				
Start Date: 1996-01-01	Start Hour: 1	End Date: 2000-12-31	End Hour: 24	

#### Wind Speed Categories

Stability Category	Wind Speed [m/s]	Stability Category	Wind Speed [m/s]
A	1.54	D	8.23
В	3.09	E	10.8
С	5.14	F	No Upper Bound



### Results Summary - NO2 (1hr)

D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.isc

NO2 - Concent	102 - Concentration - Source Group: BACKGRND												
Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour				
1-HR	1ST	25.10000	ug/m^3	488294.31	5371363.28	348.00	1.80	348.00					
1-HR	8TH	25.10000	ug/m^3	488294.31	5371363.28	348.00	1.80	348.00					

#### NO2 - Concentration - Source Group: NETRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
1-HR	1ST	48.90890	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	
1-HR	8TH	44.48384	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	

#### NO2 - Concentration - Source Group: ROADS

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
1-HR	1ST	1.37054	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	
1-HR	8TH	1.36859	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	

#### NO2 - Concentration - Source Group: SWTRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
1-HR	1ST	50.64791	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	
1-HR	8TH	44.42121	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h1.isc AERMOD View by Lakes Environmental Software

RS - 1 of 1



### Results Summary - NO2 (24hr & Annual)

D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.isc

NO2 - Concentration - Source Group: BACKGRND												
Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour			
24-HR	1ST	22.70000	ug/m^3	488294.31	5371363.28	348.00	1.80	348.00	1996-01-05, 24			
ANNUAL		22.70000	ug/m^3	488294.31	5371363.28	348.00	1.80	348.00				

#### NO2 - Concentration - Source Group: NETRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	5.11073	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	1998-12-30, 24
ANNUAL		0.84080	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	

#### NO2 - Concentration - Source Group: ROADS

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	1.19314	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	
ANNUAL		0.33686	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	

#### NO2 - Concentration - Source Group: SWTRAIN

Averaging Period	Rank	Peak	Units	х (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	4.03115	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	1997-01-06, 24
ANNUAL		0.79037	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\NO2h24.isc AERMOD View by Lakes Environmental Software

RS - 1 of 1



### Results Summary - PM2.5 (24hr & Annual)

D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.isc

PM-2.5 NAAQS - Concentration - Source Group: NETRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.55375	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	
24-HR	8TH	0.28448	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	
ANNUAL		0.07916	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	

#### PM-2.5 NAAQS - Deposition - Source Group: NETRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
ANNUAL		0.00417	g/m^2	488202.59	5371246.31	348.00	1.80	348.00	

#### PM-2.5 NAAQS - Concentration - Source Group: ROADS

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.02079	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	
24-HR	8TH	0.01657	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	
ANNUAL		0.00663	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	

#### PM-2.5 NAAQS - Deposition - Source Group: ROADS

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
ANNUAL		0.00037	g/m^2	488059.75	5371288.11	348.00	1.80	348.00	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

RS - 1 of 2



## **Results Summary**

D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.isc

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.54145	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	
24-HR	8TH	0.27730	ug/m^3	488266.82	5371302.96	348.00	1.80	348.00	
ANNUAL		0.07562	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	

#### PM-2.5 NAAQS - Deposition - Source Group: SWTRAIN

Averaging Period	Rank	Peak	Units	x (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
ANNUAL		0.00445	g/m^2	488202.59	5371246.31	348.00	1.80	348.00	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\PM25h1.isc AERMOD View by Lakes Environmental Software

RS - 2 of 2



#### Results Summary Benzene (24hr & Annual)

D:\Projects\2024\24120 Timmins\AERMOD\NO2NAAQS1h.isc

BENZENE - Concentration - Source Group: NETRAIN									
Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.01453	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	1998-02-19, 24
24-HR	8TH	0.00999	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	1996-01-07, 24
ANNUAL		0.00213	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	

#### BENZENE - Concentration - Source Group: ROADS

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.00220	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	
24-HR	8TH	0.00189	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	1997-01-02, 24
ANNUAL		0.00062	ug/m^3	488059.75	5371288.11	348.00	1.80	348.00	

#### BENZENE - Concentration - Source Group: SWTRAIN

Averaging Period	Rank	Peak	Units	X (m)	Y (m)	ZELEV (m)	ZFLAG (m)	ZHILL (m)	Peak Date, Start Hour
24-HR	1ST	0.01061	ug/m^3	488101.40	5371322.27	348.00	1.80	348.00	1996-01-03, 24
24-HR	8TH	0.00827	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	1997-09-12, 24
ANNUAL		0.00250	ug/m^3	488202.59	5371246.31	348.00	1.80	348.00	

Project File: D:\Projects\2024\24120 Timmins\JANUARY 8 2025\Benzeneh24.isc AERMOD View by Lakes Environmental Software

RS - 1 of 1







**MOVES4** Emissions Rates



## Appendix B – MOVES4 Emission Rates

<ol> <li>Make Choices in MOVES program.</li> </ol>	
g leg for beneficient production (beneficient of beneficient) g leg for beneficient (beneficient) v leg for beneficient v leg for ben	
Rank Strom. © Monte Conservation Statute Strom	Choose a weekday in January and another in July.
ands to real.	Chippewa County MI. is the closest US to Timmins.
✓ Odput Imaxims State     One-Odds       © even input Database     Image: Control of the Control o	









With all checkmarks, can choose Execute from Action tab.

When run is done, go to Post Processing Run Sql Script - choose EmissionRates.sql.

Then run Post Summary Report. Choose your run, then source 1st, fuel 2nd, then the contaminant of interest, either Benzene, NOX or PM2.5. For each source, proportion the emission per vehicle by fuel in each of the three (Benzene, NOX and PM2.5) spreadsheets.

Use Ontario Fleet information for Passenger Car, Passenger Truck & SUV, Short and Long-Haul Trucks, and Busses.







Fugitive Dust Best Management Plan



## Appendix C – Fugitive Dust Best Management Plan

## Fugitive Dust "Best Management" Plan for Timmins-Porcupine Station Construction Phase, Timmins Ontario

US EPA AP-42 13.2.3 (Heavy Construction Operations) estimates construction emissions as primarily fugitive dust emitted at a rate of 2,690,000 g/hectare/month. The site is approximately 0.8 hectares, resulting in an average emission of 0.91 g/s. The following describes the dominant sources of fugitive dust and dust management strategies.

### 1. Potential Sources of fugitive dust at this site:

- Demolition and debris removal,
- Site Preparation,
- General Construction,

### 2. Composition and size range of fugitive dust:

Dust generated from the potential sources at this site will likely generally lack contaminants other than particulate. Further, a significant portion of the fugitive dust from these sources is coarse and only a small fraction is dust in the respirable range.

According to USEPA AP-42 13.2.4-4, 74% of the fugitive dust particles are smaller than 30um, 48% are smaller than 15um, 35% are smaller than 5um, and 0.53% are smaller than 2.5um, the ultimate size fraction considered respirable. According to regulation 419/05 the suspended particulate limit is  $120ug/m^3$  (24h - Schedule 3) and is based on visibility, however, respirable particles (2.5um and less) can penetrate deep into the respiratory system and as a result pose concerns with regard to health.

### 3. Fugitive Dust Control Actions:

Depending on the source, there are a variety of measures used to reduce the impact of fugitive dust emissions. These are discussed for each source in the following.

## 3.1 Truck transport

To achieve a good level of control the following actions should be followed:

- Roads should be sprayed with water and/or treated with appropriate chemical agents, at frequencies as required to control fugitive dust emissions resulting from vehicular travel, and
- Vehicle speeds on internal haul roads should be limited



- Ensure trucks hauling aggregates are tarped, and
- Establish efficient traffic patterns to minimize dust generation.

### 3.2 Debris Handling

Fugitive dust is controlled when loading trucks with water sprays and strategically located wind barriers to speed reduce the wind speed.

### 3.3 Bulldozers

Wet suppression is recommended for areas to be bulldozed. Excavated materials may already be moist and not require additional wetting.

### 3.4 Pan Scrapers

Wet suppression of travel routes is recommended for areas to be scraped.

### 3.5 Cut / Fill Material

Fugitive dust is controlled with water sprays and strategically located wind barriers to reduce the wind speed.

### 3.6 Cut / Fill Haulage

To achieve a good level of control the following actions (similar to debris handling) should be followed:

- Roads should be sprayed with water and/or treated with appropriate chemical agents, at frequencies as required to control fugitive dust emissions resulting from vehicular travel, and
- Vehicle speeds on internal haul roads should be limited
- Ensure trucks hauling aggregates are tarped, and

Establish efficient traffic patterns to minimize dust generation.

### 3.7 General Construction

Fugitive dust can be controlled with strategically located wind barriers to reduce the wind speed, wet suppression, and early paving of permanent roads.



# 4. Record Keeping

A daily log of water and other dust control procedures and observations should be kept at the site to demonstrate, if necessary, that dust control actions are being taken.

## 5. Response to Complaints

Complainants are to be requested to provide information as required to complete a record of environmental complaint response that upon completion will be sent to the Site Manager. The Site Manager will:

- 1. Investigate the site and circumstances leading to said emissions of dust driving the complaint, and
- 2. Determine if the source of the dust complaint was indeed the result of operations, and if so
- 3. Adjust or modify fugitive dust mitigation systems as required to prevent a reoccurrence, and if necessary
- 4. Review the Dust Management Plan and implement additional control measures as necessary,
- 5. Respond to the Complainants in a timely manner, and
- 6. Document the resulting information in an on-site log that will be made available to the MECP upon request.

A sample form is included below.

### 6. Conclusion

The monitoring and control measures of this Dust Management Plan are intended to meet or exceed industry standards for controlling fugitive dust emissions resulting from the construction phase. The measures will be implemented as required to control emissions from construction.



### **RECORD OF ENVIRONMENTAL COMPLAINT RESPONSE**

1.	Location:
2.	Date and Time Complaint Received:
3.	Name of Complainant:
Addı	ress:
Tele	phone Number:
4. Othe	Form of Complaint: Visit:[] Telephone Call:[] Letter:[] Attach Copy
5	Complaint Referred to Technical Services: No:[] Yes:[] and provide details:
6.	Complaint Made with Government Official(s): No:[] Yes:[] If Yes, Attach Record of MECP Letter
7.	Details Concerning Investigation Made by Company Concerning Complaint:
8.	Response to Complaint:         Letter:[]Date Attach copy of letter to form.         Telephone Call:[]Date Time         Summary of Telephone Call:
9.	Follow-up Action Taken by Company: None:[] Details:
10	. Filed a copy of this Form in Plant Environmental Manual: Yes:[]
	Date:

Employee Signature, Name & Position

